

Topic 6. Radiation Fundamentals

Telecommunication Systems Fundamentals

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Concepts in this Chapter

- *Antennas: definitions and classification*
- *Antenna parameters*
- *Fundamental Theorems: uniqueness and reciprocity. Images' method*
- *Friis' equation*
- *Link Budget of a Radio-Link*

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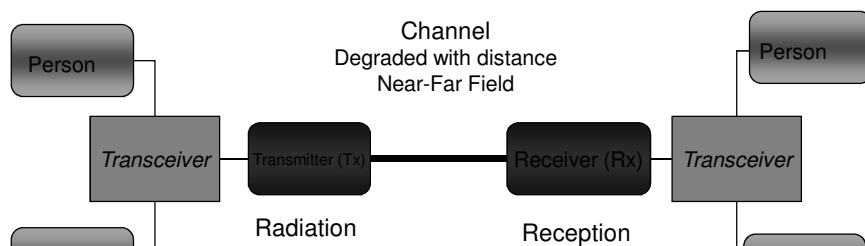
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Bibliography

Antenna Theory and Design. W.L. Stutzman, G.A. Thiele.
John Wiley & Sons

Introduction: Radio-Telecommunication Systems

- Info transmission implies to transmit a signal (with a given energy) through a radio-channel



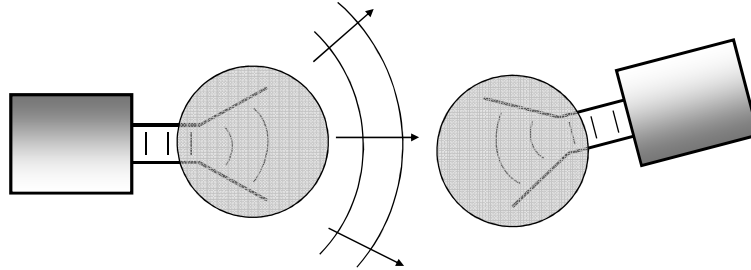
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Introduction: Transmitting and Receiving Antenna

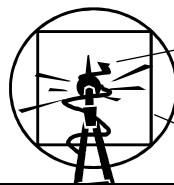
- An antenna can either transmit (radiate) energy in Transmission



- Or capture energy in Reception

Radiation Performance of an Antenna

- Radiation is the electromagnetic energy flux outward from a source
- Basic Problem in electromagnetic theory:
 - Calculus of the electromagnetic field produced by a structure in any given space point



From Electrical Currents within the Tx'ing antenna structure

From the Electromagnetic Field distribution along a closed surface

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Efficiency as Main Objective in Antennas

- Efficiency is the main objective when designing/ selecting an antenna
 - Maximize the electromagnetic field power in a given point given an amount of power provided to the antenna
- Which antenna parameters should we consider
 - Phase Center
 - Power Parameters
 - » Radiated power flux density
 - » Radiation intensity
 - » Directivity
 - » Power Gain
 - Gain diagram
 - Polarization
 - Bandwidth

Power Parameters: Poynting's Theorem

- **Complex Poynting's Vector:** electromagnetic energy flux density through a given surface

$$S = \frac{1}{2} \operatorname{Re}\{\bar{E} \times \bar{H}^*\}$$

- **Average Power:** Poynting's vector flux

$$P_{\text{media}} = \iint S \cdot dS \text{ [W]}$$

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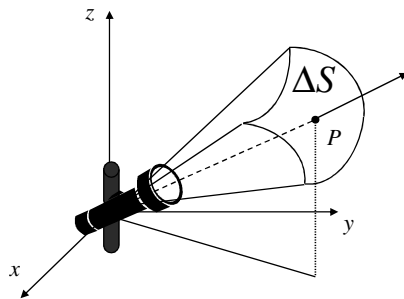
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Power Parameters: Radiation Density

- Average radiated power **per surface unit** in a given direction

$$\phi(\theta, \varphi) = \frac{1}{2} \operatorname{Re}\{\bar{E} \times \bar{H}^*\} \left[\frac{W}{m^2} \right]$$



$$\phi(\theta, \varphi) = \frac{\Delta p(\theta, \varphi)}{\Delta S}$$

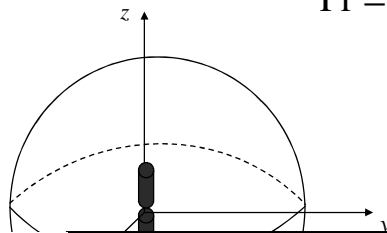
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Power Parameters: Radiated Power

- **Sum up** radiated flux density along a sphere surface that circumscribe the antenna

$$Pr = \iint \phi(\theta, \varphi) \cdot dS \text{ [W]}$$



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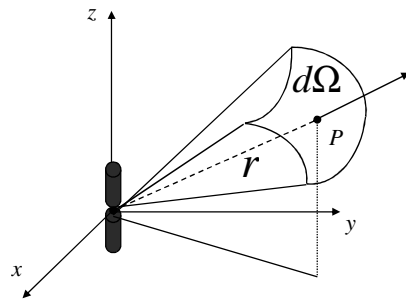
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Power Parameters: Radiation Intensity

- Average radiated power **per solid angle unit** in a given direction

$$i(\theta, \varphi) = \frac{\Delta p(\theta, \varphi)}{\Delta \Omega} \left[\frac{W}{\text{esteroradian}} \right]$$



$$Pr = \iint i(\theta, \varphi) \cdot d\Omega$$

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Power Parameters: Radiation Intensity

- **Independently of the distance** from the antenna

$$\Delta S = r^2 \Delta \Omega \Rightarrow \phi(\theta, \varphi) \cdot r^2 = i(\theta, \varphi)$$

- The Power Flux Density decreases with distance inversely proportional to the area of the spherical solid angle

$$r(\theta, \varphi) = \frac{i(\theta, \varphi)}{i_{\max}}$$

- Radiation Diagram (power-wise)

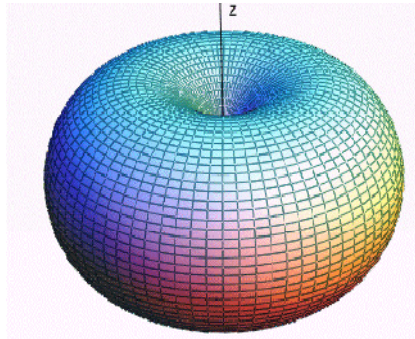
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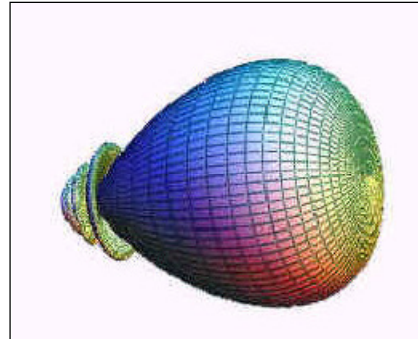
Power Parameters: Radiation Intensity

Omnidirectional (on Azimuth)



Dipolo: typical on cellular terminals

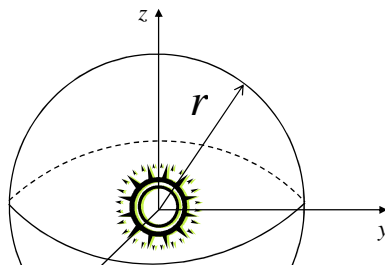
Directive



Yagi: typical for television receivers

Power Parameters: Isotropic Antenna

- **Ideal** point source that radiates **uniformly** in all directions



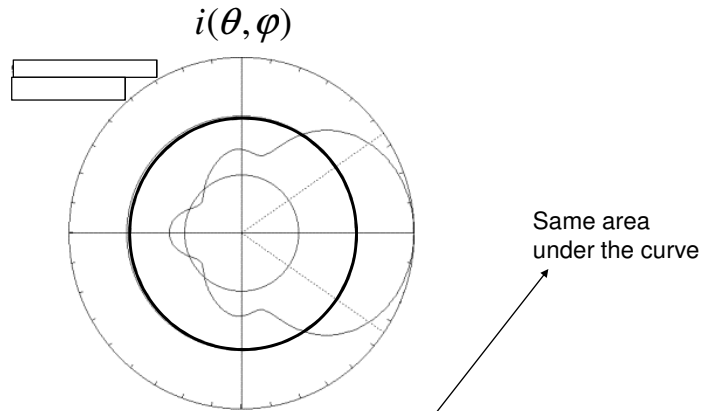
$$i_{iso} = \frac{Pr}{4\pi}$$
$$\phi_{iso} = \frac{Pr}{4\pi \cdot r^2}$$

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Power Parameters: Isotropic Antenna



Assuming the same transmitted power by both antennas...which *focalizes* better?

Power Parameters: Directivity (function of direction)

- Ratio between the power density flux an antenna radiates and the one an isotropic (omnidirectional) antenna would do, as a function of the radiating direction

$$D(\theta, \varphi) = \frac{i(\theta, \varphi)}{i_{iso}} = 4\pi \frac{i(\theta, \varphi)}{Pr}$$

Pr

Pr

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Power Parameters: Directivity

- Directivity is defined as the maximum value of the Directivity function

$$D = 4\pi \frac{i_{\max}}{Pr}$$

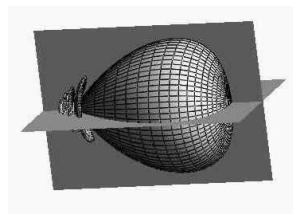
– Because $Pr = \iint i(\theta, \varphi) \cdot d\Omega$ $r(\theta, \varphi) = \frac{i(\theta, \varphi)}{i_{\max}}$

$$D = \frac{4\pi}{\Omega_A} \quad \text{being} \quad \Omega_A = \iint r(\theta, \varphi) d\Omega$$

Power Parameters: Directivity

- When the Beam is narrow

$$D \approx \frac{4\pi}{\theta_1 \theta_2}$$



- Conclusions

- Directivity provides information about how the radiated power is distributed with direction (elevation and azimuth)
- Directivity does not provide information about the actual

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Power Parameters: Gain Function

- **Ratio** between the power intensity radiated in a direction and the radiated intensity of an isotropic antenna, given a power available to the antenna

$$G(\theta, \varphi) = 4\pi \frac{i(\theta, \varphi)}{P_{in}}$$

being P_{in} the power available at the antenna input

Power Parameters: Gain

- Gain is the maximum value of the Gain Function

$$G = 4\pi \frac{i_{\max}}{P_{in}}$$

- Because it is a ratio, the units are dBs

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Power Parameters: Examples of Gain

ANTENNA TYPE	GAIN (dBi)
Isotropic	0,0
Ground Plane 1/4 wavelength	1,8
Dipole 1/2 wavelength	2,1
Monopole 5/8 wavelength	3,3
Yagui 2 elements	7,1
Yagui 3 elements	10,1
Yagui 4 elements	12,1
Yagui 5 elements	14,1

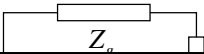
Power Parameters: Efficiency

- P_{in} and P_r are related to each other around radiating **Efficiency** of the antenna

$$P_r = \eta \cdot P_{in}$$

$$\eta_{cd} = \frac{R_r}{R_r + R_L}$$

$$\eta_d = 1 - |\Gamma|^2$$

$$\Gamma = \frac{Z_a - Z_g}{Z_a + Z_g}$$


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Power Parameters: Efficiency

- From the above definition of Efficiency, the relationship between Gain and Directivity of an antenna can be derived

$$G = \eta \cdot D$$

- Can the Gain of an antenna be increased by increasing the Directivity?

Example

- A dipole of half wavelength without losses, with input impedance of 73Ω is connected to a transmission line with characteristic impedance of 50Ω . Assuming the radiating intensity of the antenna is

$$i(\theta) = B_0 \sin^3(\theta)$$

Compute the Gain of the Antenna

$$i_{\max} = i_{\max}(\theta) = B_0$$
$$P = \int_0^{2\pi} \int_0^{\pi} D(\theta) \cos\theta \sin\theta d\theta = 3\pi^2 B_0$$

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Example Answer

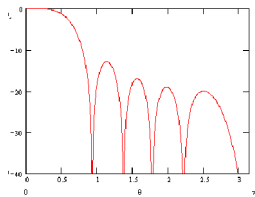
$$i_{\max} = i_{\max}(\theta) = B_0$$

$$P_r = \int_0^{2\pi} \int_0^{\pi} D(\theta) \sin \theta = 2\pi B_0 \int_0^{\pi} \sin^4 \theta d\theta = B_0 \left(\frac{3\pi^2}{4} \right)$$

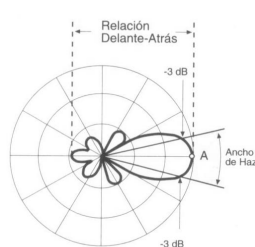
$$D = 4\pi \frac{i_{\max}}{P_r} = 1.697$$

$$G = \eta \cdot D = (1 - |\Gamma|^2) D = \left(1 - \left| \frac{73 - 50}{73 + 50} \right|^2 \right) 1.697 = 0.965 \cdot 1.697 = 1.638 = 2.14 \text{ dB}$$

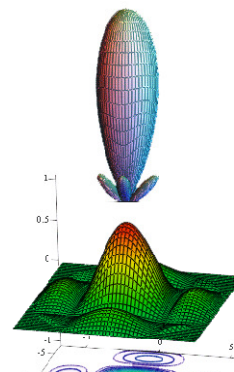
Radiation Diagram



Cartesian



Polar



What parameter are usefull?

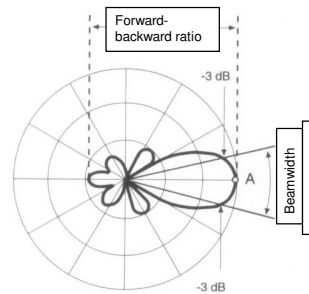
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Radiation Diagram

- Parameters to characterize the lobe structure
 - Beamwidth
 - Null to Null Beamwidth
 - Half Power Beamwidth (HPBW) – 3dBs
 - 10 dB Beamwidth
 - Lobes
 - Main lobe
 - Side lobes
 - First lobe
 - Backlobe
 - Forward-backward ratio



Radiation Diagram: Classification

- Isotropic
- Omnidirectional
- Directive
- Multi-beam

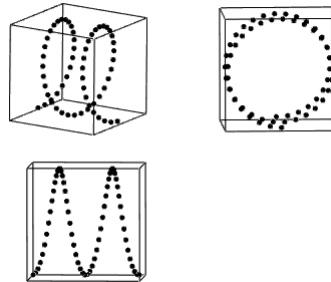
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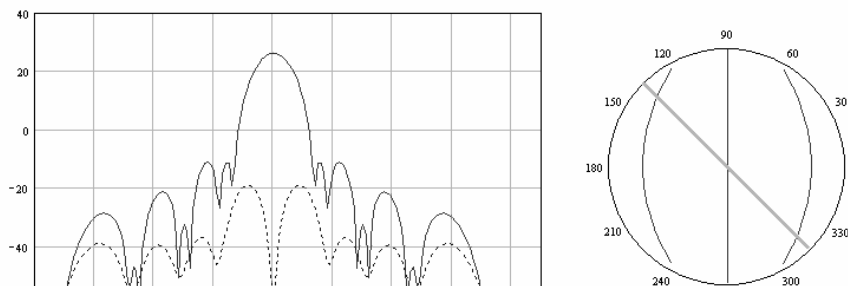
Polarization

- Of a **Plane-wave**, it refers to the spatial orientation of the time-variation of the electric field
- Of an **antenna**, it refers to the polarization of the radiated field
 - Generally speaking polarization is defined according to the propagation direction



Polarization

- Co-Polar and Cross-Polar components



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Antenna Bandwidth

- Frequency margin where the defined parameters for the antenna remain valid (impedance, beamwidth, sidelobes ratio, etc.)
 - Narrowband Antennas (<10% central frequency)
 - Broadband Antennas (>10% central frequency)

Antenna Radiation on Free-Space Condition

- What is Free-Space condition: no obstacles or material to influence the radiation pattern – not even the ground



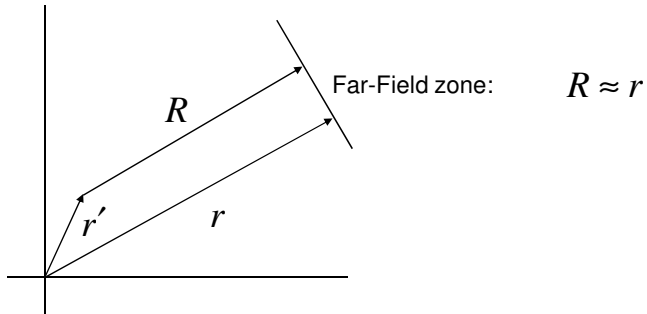
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Radiation Zones

- When the distance is much greater than the wavelength, $R \gg \lambda$, the observed wave behaves as a Plane-Wave.
- When can we consider we are “far enough”?

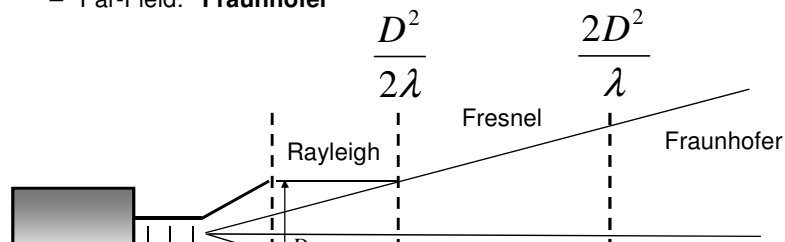


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Radiation Zones

- Simplifying but useful approach: three zones are defined:
 - Near-Field: **Rayleigh** (spheric propagation)
 - Intermediate-Field: **Fresnel** (interferences)
 - Far-Field: **Fraunhofer**



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Radiation Zones: Far-Field

- Conclusions:
 - Power decreases as **square of the distance**
 - Satisfy condition of **Plane-Wave**
 - E and H fields are perpendicular
 - Amplitude of E and H fields are related to each other through the transmission mean impedance
 - The type of the transmitting antenna affects only on the angular variation of the transmitted power flux (**Radiation Diagram**)
 - **Transmission direction of the wave propagation** coincides with **line of sight** of the transmitting antenna

EIRP - Equivalent Isotropic Radiated Power

- The product of the antenna Gain by the available Power

$$PIRE = G \cdot P_{in}$$

$$i_{iso} = \frac{P_{in}}{4\pi}$$

$$i_{ant} = \frac{G \cdot P_{in}}{4\pi} = \frac{PIRE}{4\pi}$$



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EIRP

- Its units are dBW (or dBm)
- We will see later, this parameter (expressed on dBW) is quite useful when computing the “availability” of the radio-link
- Example: if the Gain of an antenna is 2dBi and it gets a power of 10W, How much is its EIRP?

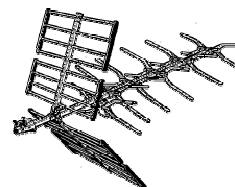
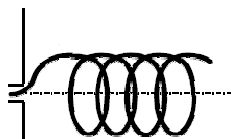
$$G = 2 \text{ dB}$$

$$P_{in} = 10 \cdot \log(10) = 10 \text{ dB}$$

$$PIRE = 12 \text{ dB}$$

Lineal Antennas

- Antennas built with thin electrically conductive wires (very small diameter compared to λ).
- They are used extensively in the MF, HF, VHF and UHF bands, and mobile communications.
- Among others:
 - Dipole
 - Monopole
 - Yagi antenna
 - Loops



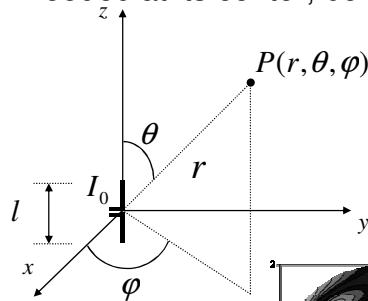
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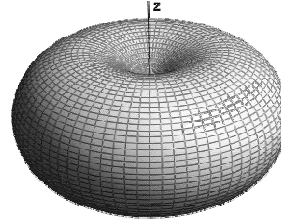
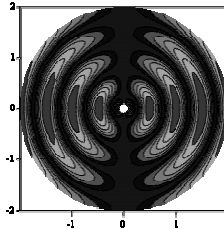
Lineal Antennas: Infinitesimal Dipole

- Formed by two short conductive wires simetrically feeded at its center, being $l \ll \lambda$.



$$E_{\theta} = jZ_0 \frac{l \cdot I_0}{2\pi \cdot \lambda \cdot r} \text{sen}(\theta) \cdot e^{-j\frac{2\pi}{\lambda}r}$$

With Linear Polarization
And radiation diagram



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Lineal Antennas: Infinitesimal Dipole

- Computing the magnetic field from the electrical, calculating the power flux and integrating for all θ we get

$$P_r = Z_0 \left(\frac{2\pi}{3} \right) \left(\frac{l \cdot I_0}{\lambda} \right)^2 = I_0^2 R_r$$

$$R_r = 80\pi^2 \left(\frac{l}{\lambda} \right)^2$$

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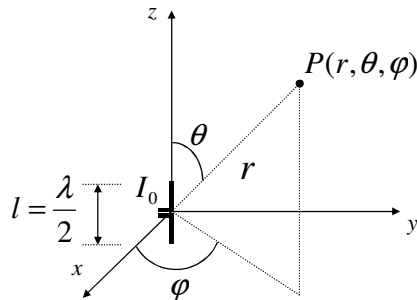
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Lineal Antennas: Half-Wavelength Dipole

- Very common antenna, with a “convenient” radiation impedance of 73Ω



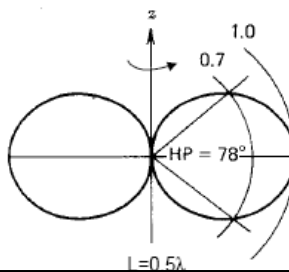
$$E_{\theta} = jZ_0 \frac{I_0 e^{-j\frac{2\pi}{\lambda}r}}{2\pi \cdot r} \left[\frac{\cos\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} \right]$$

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Lineal Antennas: Half-Wavelength Dipole

- Radiation parameters



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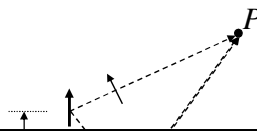
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Radiated Field over a Perfect Conductor

- Up to this point we have assumed the antennas are in the free-space environment. However they usually are close to the ground
- When the distance to ground is comparable to the wavelength, and the beamwidth is large, antenna radiation is heavily affected by the presence of the ground
- For these scenarios, we will assume the ground is a perfect conductor, infinite and plane

Image Theory

- Intuitively, the field is reflected on the ground
 - Perfect conductor: the transmitted wave is reflected
 - The field P is the result of the sum of the direct and reflected waves
 - Field P is the result of the primary and image waves in the equivalent free-space scenario
 - Which is valid only for the upper half semi-space



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Image Theory

- Example: field produced by a Infinitesimal dipole

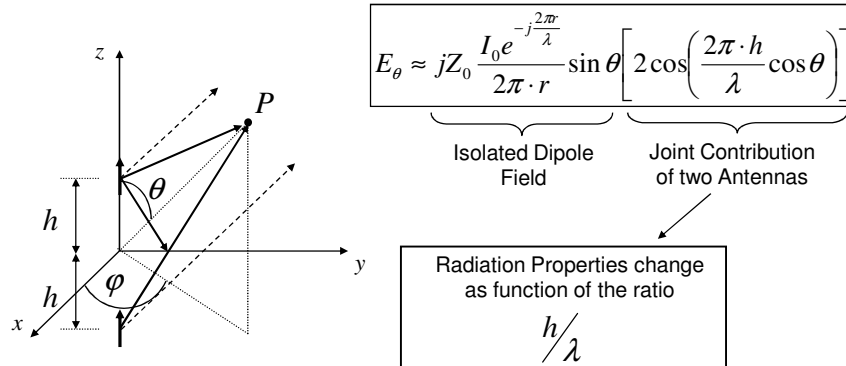
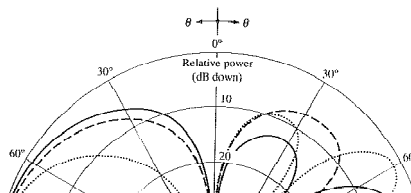


Image Theory

- Example (cont.)
 - If $\lambda \gg h$ then, directivity increases by 3dB! -> decrease the size
 - Otherwise....



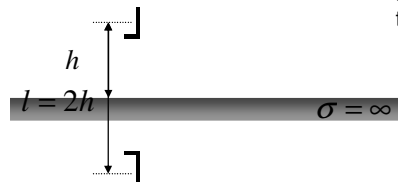
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Monopole

- Vertical Dipole divided to its half, that is fed between wire end and a conductive plane



- Applying Image theory, it can be proven that a monopole above a conductive plane exhibit the same behavior than a dipole with a length twice the height of the monopole

Consider only $z > 0$ and $\lambda \gg h$

$$Pr_{mono} = \frac{1}{2} Pr_{dipolo}$$

$$R_{r,mono} = \frac{1}{2} R_{r,dipolo}$$

$$i_{mono} = i_{dipolo}$$

$$D_{mono} = 2D_{dipolo}$$

Monopole

- Example: $\lambda/4$ monopole
 - As shown before, the monopole exhibit the same performances than a $\lambda/2$ dipole and therefore its directivity is

$$D = 5.15 \text{ dBi}$$

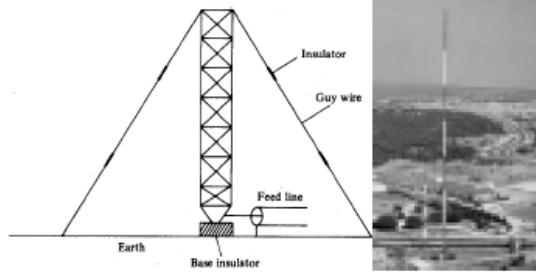
- At low frequencies, this antenna has quite large physical dimensions
 - Example: the standard AM transmitter for frequency carrier

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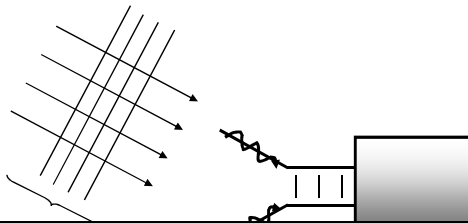
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Monopole



Reception of an Electromagnetic Field

- If an electromagnetic wave, with a plane-wave like propagation, runs over a conductor (antenna) it generates a current distribution over it



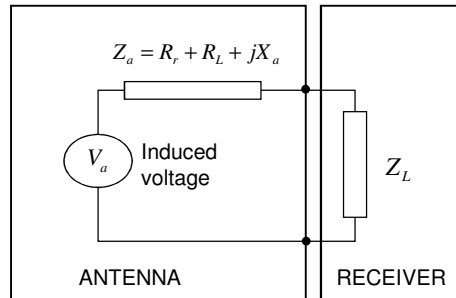
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Equivalent Circuit Model for a Receiving Antenna

- An antenna at reception is designed to optimize the power handed out at its terminal



- Available power at antenna

$$P_a = \frac{|V_a|^2}{8R_a}$$

- Power handed out

$$P_L = \frac{1}{2} |I_L|^2 R_L = P_a (1 - |\Gamma|^2)$$

$$\Gamma = \frac{Z_a - Z_L}{Z_a + Z_L}$$

Reciprocity Theorem

- It allows to relate the properties of an antenna when receiving and transmitting
- “The relationship between an oscillating current and the resulting electric field is unchanged if one interchanges the points where the current is placed and where the field is measured”
 - For the specific case of an electrical network, it is sometimes phrased as the statement that voltages and currents at different points in the network can be interchanged”

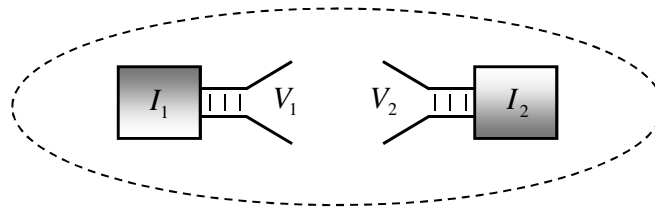
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Reciprocity Theorem

- Suppose an anechoic chamber (no echo) in which are placed two antennas, both can transmit and receive, and operating at the same frequency



- The roles of sending and receiving can be exchanged. Thus, the radiation patterns of transmitting and receiving are the same

$$\text{If } I_1 \rightarrow V_{2,ca} \Rightarrow V_{1,ca} = V_{2,ca} \text{ when } I_2 \rightarrow V_{1,ca}$$

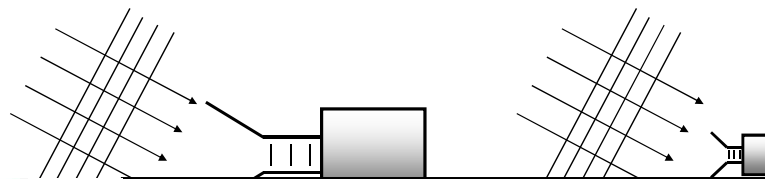
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$$I_1 = I_2$$

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Effective Aperture

- Effective Aperture of an antenna characterizes the electromagnetic energy that it is able to capture
- Intuitively a large antenna captures more power, as it has more area



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Effective Aperture

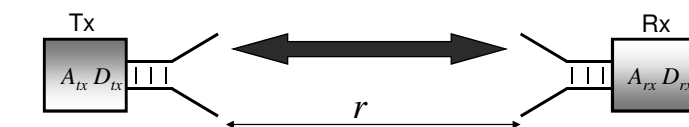
- Equivalent aperture is defined as

$$A_{ef} = \frac{\text{Potencia entregada}}{\text{Densidad de potencia incidente}} = \frac{P_L}{\phi_i} = \frac{|I_L|^2 R_L / 2}{\phi_i}$$

- The value does not have to match the dimensions (physical) of the antenna.
- When the antenna is flat, the physical relationship between the opening (A_f) and the effective aperture (A_{eff}) is known as aperture efficiency, verifying that:

$$A_{eff} = \varepsilon_{ap} A_f \quad \text{con } 0 \leq \varepsilon_{ap} \leq 1$$

Directivity vs Maximum Effective Aperture



$$\phi_{tx} = \frac{P_{tx}}{4\pi \cdot r^2} D_{tx}$$

$$P_{rx} = \phi_{tx} A_{rx} = \frac{P_{tx} D_{tx} A_{rx}}{4\pi \cdot r^2} \longrightarrow D_{tx} A_{rx} = \frac{P_{rx}}{P_{tx}} (4\pi \cdot r^2)$$

$$D_{rx} A_{tx} = \frac{P_{tx}}{P_{rx}} (4\pi \cdot r^2)$$

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Directivity vs Maximum Effective Aperture

$$\frac{D_{tx}}{A_{tx}} = \frac{D_{rx}}{A_{rx}} \Rightarrow \frac{D_{tx}}{A_{tx,m}} = \frac{D_{rx}}{A_{rx,m}}$$

- The above solution is valid for any antenna. For an infinitesimal dipole it can be proof that

$$A_{ef} = \frac{3\lambda^2}{8\pi} = \frac{\lambda^2}{4\pi} D$$

Directivity vs Maximum Effective Aperture

- In case of losses associated to the antenna, the maximum effective aperture is

$$A_{ef} = \eta_{cd} (1 - |\Gamma|^2) \frac{\lambda^2}{4\pi} D = \frac{\lambda^2}{4\pi} G$$

$$G = \frac{4\pi}{\lambda^2} A_{ef}$$

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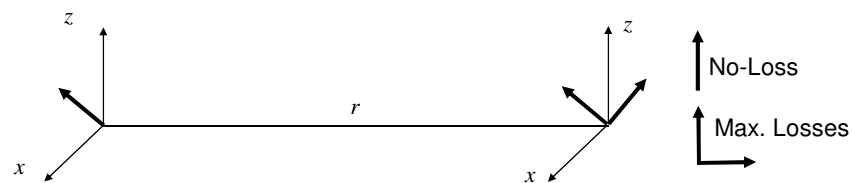
Polarization Mismatch

- The difference of polarization between transmitting and receiving antennas, it is known as **Polarization Loss Factor**

$$L_{polarization} = |\bar{e}_{tx} \cdot \bar{e}_{rx}^*|^2$$

Polarization Vector
For Tx antenna

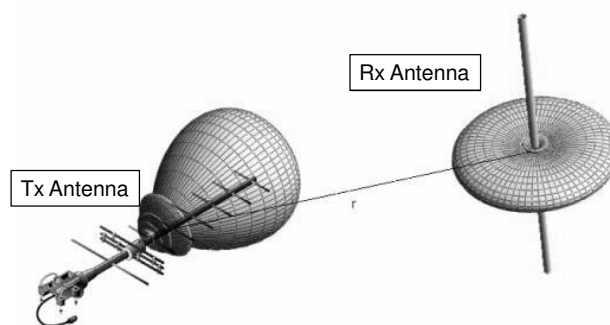
Polarization Vector
For Rx antenna



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Gains in the Radio Link: Tx and Rx Gains



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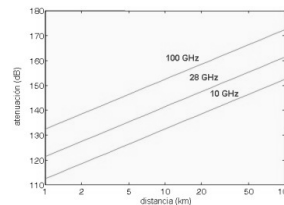
Friis Transmission Equation

- For Isotropic antennas and free-space propagation
 → The basic losses are

$$\left. \begin{aligned} P_{Rx} &= \phi_{iso} \cdot S_{eq_{iso}} = \phi_{iso} \cdot \frac{\lambda^2}{4\pi} \\ \phi_{iso} &= \frac{P_{Tx}}{4\pi d^2} \end{aligned} \right\} \Rightarrow l_{bf} = \frac{P_{Tx}}{P_{Rx}} = \left(\frac{4\pi d}{\lambda} \right)^2$$

$$L_{bf}(dB) = 32,45 + 20 \log f(MHz) + 20 \log d(km)$$

$$L_{bf}(dB) = 92,45 + 20 \log f(GHz) + 20 \log d(km)$$



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Friis Transmission Equation

- For any pair of antennas and free-space propagation
 → The basic losses are

$$\left. \begin{aligned} l_{bf} &= \frac{P_{et}}{P_{dr}} \left\{ \begin{array}{l} P_{et} : \text{power handed in to Tx antenna} \\ P_{dr} : \text{power handed in to Rx antenna} \end{array} \right. \\ P_{dr} &= \phi \cdot S_{eq} = \phi \cdot \frac{\lambda^2}{4\pi} \cdot g_{Rx} \\ \phi &= \frac{P_{et}}{4\pi d^2} \cdot g_{Tx} \end{aligned} \right\} \Rightarrow l_{bf} = \frac{P_{Tx}}{P_{Rx}} = \left(\frac{4\pi d}{\lambda} \right)^2 \cdot \frac{1}{g_{Tx} \cdot g_{Rx}} = \frac{l_{bf}}{g_{Tx} \cdot g_{Rx}}$$

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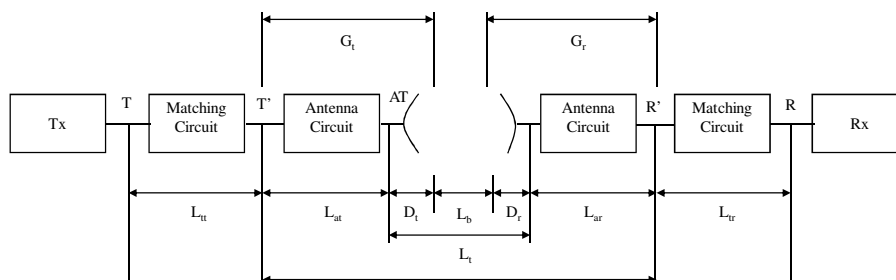
Friis Transmission Equation

- Sumarizing, for any antenna

$$l_t = \frac{p_{Tx}}{p_{Rx}} = a_e \cdot \left(\frac{4\pi d^2}{\lambda} \right) \cdot \frac{1}{g_{Tx} \cdot g_{Rx}} \quad \boxed{L_t = L_{bf} + A_e - G_t - G_r = L_b - G_t - G_r}$$

	Usual Notation	Definition	
		Antennas	Mean
Free-Space Basic Loss	L_{bf}	Isotropic	Free-Space
Basic Loss	L_b	Isotropic	Any
Free-Space Transmission Loss	L_{tf}	Any	Free-Space
Transmission Loss	L_t	Any	Any

Friis Transmission Equation



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Link Budget

- Link Budget = expression for available power at the receiver as a function of
 - Transmitted Power
 - Rx and Tx Antenna Gains
 - All the losses in the link

$$P_{Rx} = P_{Tx} - L_{bf} + G_{Tx} + G_{Rx} - A_e$$

Link Budget

- Other factors affecting the link
 - Normalized Noise Power
 - SNR
 - Power-limited Systems
 - Minimum Received Power (Sensibility) + Fading Margin
 - The maximum distance between Tx and Rx is calculated by the Link Budget

$$p_n = k \cdot T_0 \cdot b \cdot f_{sis} \quad P_n (dBm) = F_{sis} (dB) + 10 \log b (Hz) - 174$$

- Interference

$$p_n = k \cdot T_{eq} \cdot b$$

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Important Concepts in this Topic

- Poynting Vector
- Radiated Power Flux Density
- Antenna Directivity
- Antenna Gain
- Antenna Efficiency
- Antenna Effective Aperture
- Polarization
- Reciprocity Theorem
- Most common simple antennas
- Friis Equation and Link Budget
- Free-Space Basic Propagation Loss

The logo for Cartagena99 features the text 'Cartagena99' in a stylized, teal-colored font. The '99' is significantly larger and more prominent than the 'Cartagena' part. The text is set against a light blue background with a white, stylized wave or arrow shape pointing to the right. Below the text, there is a horizontal orange and yellow gradient bar.

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