



$$\eta_v = \frac{V_{ext} \rho_0}{Q \rho_F} \frac{\rho_A}{\rho_0} = \frac{\rho_A}{\rho_0} (1 + \alpha) - \alpha$$

MASA QUE ENTRA  $(1 + \alpha) Q \rho_F - \alpha Q \rho_0$

$$V = Q \left[ \alpha + \sin\left(\frac{\pi}{2} \zeta\right) \right],$$

CONTINUIDAD:  $\frac{d}{dt} \int_V \rho dV + \int_{\Sigma_c} \rho(\vec{v} - \vec{v}_c) \cdot \vec{n} d\sigma = 0 \rightarrow \left[ \frac{d}{dt} \rho V = G \right]$

$t=0, \rho = \rho_0, P = P_0$

ENERGIA:  $\frac{d}{dt} \left[ \int_{V_c} \rho e dV \right] + \int_{\Sigma_c} \rho \left( e + \frac{v^2}{2} \right) (\vec{v} - \vec{v}_c) \cdot \vec{n} d\sigma = - \int_{\Sigma_c} P \vec{v} \cdot \vec{n} d\sigma \rightarrow \frac{d}{dt} (\rho e V) = G h_0 - P \frac{dV}{dt} \rightarrow \left[ \frac{d}{dt} (P V) = \gamma G \frac{P}{\rho_0} - (\gamma - 1) P \frac{dV}{dt} \right]$

$$G = \rho_0 a_0 A_s \left( \frac{z}{r-1} \right)^{1/2} \left( \frac{P}{P_0} \right)^{1/2} \left[ 1 - \left( \frac{P}{P_0} \right)^{\frac{\gamma-1}{\gamma}} \right]^{1/2}$$

$$G = \rho_0 a_0 A_m \left( \frac{\gamma+1}{2} \right)^{-\frac{\gamma+1}{2(\gamma-1)}}$$

SI  $P > P_{BS}$  } donde  $P_{BS}$  SE OBTIENE DE SOLUCIONAR  
SI  $P < P_{BS}$  }  $\frac{A_s}{A_m} = \left( \frac{z}{r-1} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \left( \frac{1}{2} \right)^{1/2} \left( \frac{P_0}{P_{BS}} \right)^{\frac{\gamma-1}{2\gamma}} \left[ \left( \frac{P_0}{P_{BS}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]^{-1/2}$

UTILIZANDO COMO VARIABLES ADIMENSIONALES  $\tau = \frac{t}{t_A}, \bar{\rho} = \frac{\rho}{\rho_0}, \bar{V} = \frac{V}{Q}, \bar{P} = \frac{P}{P_0}$  EL PROBLEMA SE REDUCE A

INTEGRAR

$$\bar{V} = \alpha + \sin\left(\frac{\pi}{2} \tau\right)$$

$$\bar{G} = \frac{G}{\rho_0 a_0 A_m}$$

$$\frac{d(\bar{\rho} \bar{V})}{d\tau} = \frac{\bar{G}}{\Omega}$$

$$\bar{\rho}(0) = 1$$

$$\frac{1}{\gamma} \bar{V} \frac{d\bar{P}}{d\tau} = \frac{\bar{G}}{\Omega} - \bar{P} \frac{d\bar{V}}{d\tau} \quad (2) \quad \bar{P}(0) = 1$$

(3)  $\begin{cases} \bar{G} = \frac{A_s}{A_m} \left( \frac{z}{r-1} \right)^{1/2} \bar{P}^{1/2} \left[ 1 - \bar{P}^{\frac{\gamma-1}{\gamma}} \right]^{1/2} & \text{SI } \bar{P} > \bar{P}_{BS} \\ \bar{G} = \left( \frac{\gamma+1}{2} \right)^{-\frac{\gamma+1}{2(\gamma-1)}} & \text{SI } \bar{P} < \bar{P}_{BS} \end{cases}$

ECS. DESACOPLADAS. INTEGRANDO (2) OBTENGO  $\bar{P}(\tau)$  Y POR TANTO  $\bar{G}$ . INTEGRANDO (1) OBTENGO  $\bar{S}_A = \bar{S}(1)$  Y

POR TANTO  $\eta_v = \bar{S}_A (1 + \alpha) - \alpha = \frac{1}{\Omega} \int_0^1 \bar{G} d\tau$

LA SOLUCION DEPENDE DEL REGIMEN DE GIRO A MAYES DEL PARAMETRO  $\Omega = \frac{Q/(a_0 A_m)}{t_A} \rightarrow$  TIEMPO CARACTERISTICO DE CILINDRO CON PISTON BLOQUEADO.  
 $\rightarrow$  TIEMPO DISPONIBLE PARA ADMISION

SI  $\Omega \ll 1$  (NUMERO BAJO DE RPM)

$$(2) \rightarrow \bar{G} \approx 0 \rightarrow \boxed{\bar{P} = 1}$$

EN EL CILINDRO LA PRESION SE MANTIENE IGUAL A LA EXTERNA DURANTE EL PROCESO DE ADMISION.

(1)-(2)  $\rightarrow \frac{d(\bar{\rho} \bar{V})}{d\tau} = \frac{d\bar{V}}{d\tau} \rightarrow \boxed{\bar{\rho} = \bar{S}_A (1 + \alpha) - \alpha = 1 + \alpha - \alpha = 1}$

SI  $\Omega \gg 1$  (ALTO NUMERO DE RPM)

$$(2) \rightarrow \bar{P} \bar{V}^\gamma = \alpha^\gamma$$

EVALUACION ISENTROPICA DE LA PRESION EN EL CILINDRO

$\Omega = \frac{\rho_0 Q}{\rho_0 a_0 A_m t_A} \gg 1$  EN ESTE LIMITE LA MASA QUE ENTRA DURANTE EL PERIODO DE ADMISION  $\sim \rho_0 a_0 A_m t_A$  ES DISIPOLAZIE FRENTE A LA MASA QUE CABE EN EL CILINDRO

(1)  $\rightarrow \eta_v = \frac{1}{\Omega} \int_0^1 \bar{G} d\tau, \bar{G} = f(\tau, \alpha)$  A MAYES DE (3)  $\eta_v \approx \frac{1}{\Omega} \int_0^1 \bar{G} d\tau$

COMO  $\alpha \ll 1$  LA TUBERIA ESTA CASI SIEMPRE BLOQUEADA Y REEMPLAZA  $\eta_v \approx \frac{1}{\Omega} \int_0^1 \bar{G} d\tau$   
 $\bar{P}_{BS} = \frac{1}{\gamma} \arcsen\left[\alpha \left(\bar{P}_{BS}^{-\frac{\gamma-1}{\gamma}} - 1\right)\right] \sim \alpha$   
 $\bar{P}_{BS} = \frac{1}{\gamma} \arcsen(\bar{V} - \alpha) = 0.00122$   
 $\bar{P}_{OS} = 0.0638$   
 $\bar{P}_{AS} = 0.576$

SI  $\frac{A_s}{A_m} = 3, \bar{P}_{BS} = \frac{1}{1.027} = 0.9737, \bar{V}_{BS} = \alpha \bar{P}_{BS}^{-\frac{1}{\gamma}} = 0.1019$   
 $\alpha = 0.1, \bar{P}_{OS} = \frac{1}{2.65} = 0.377, \bar{V}_{OS} = 0.2$   
 $\bar{P}_{AS} = \frac{1}{21.2} = 0.0472, \bar{V}_{AS} = 0.886$   
 $\bar{P}_A = \left( \frac{\alpha}{1 + \alpha} \right)^\gamma$

$$\eta_{BS} \leq 0.368 \alpha$$

$\bar{\tau}_1 = 0.03, \bar{V}_1 = 0.147, \bar{P}_1 = 0.583 \rightarrow$  OC NORMAL  $\rightarrow \frac{P_2}{P_0} = 0.63, M_{OC} = 2.2, \frac{A}{A_m} = 2.005$

$\bar{\tau}_2 = 0.2, \bar{V}_2 = 0.410, \bar{P}_2 = 0.139 \rightarrow$  OC. OBLICUA EN SALIDA  $\rightarrow \frac{P_2}{P_0} = 2.94, M_{OC} = 1.63, \beta = \arcsen\left(\frac{M_{OC}}{2.65}\right) = 38, \delta = 17$

$\bar{\tau}_3 = 0.7, \bar{V}_3 = 0.991, \bar{P}_3 = 0.040 \rightarrow$  EXPANSION  $\rightarrow \frac{P_2}{P_0} = 2.65, \frac{P_3}{P_0} = 2.75, \gamma(2.75) - \gamma(2.65) = 2.16^\circ$