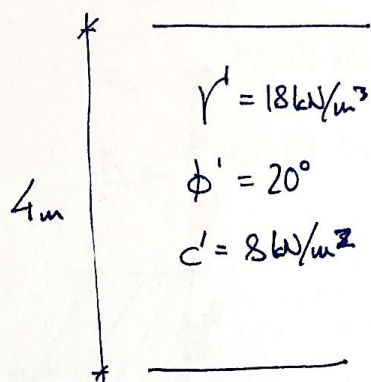


EXERCICIO 1

1



- calculamos γ'_v

$$\gamma'_v = \gamma_v = \gamma' \cdot h = 18 \text{ kN/m}^3 \cdot 4 \text{ m}$$

$$\gamma'_v = 72,00 \text{ kN/m}^2$$

- calculamos K_a

$$K_a = \frac{1 - \sin \phi'}{1 + \sin \phi'} = \frac{1 - \sin 20^\circ}{1 + \sin 20^\circ} = \frac{1 - 0,342}{1 + 0,342} = 0,49$$

- empuje sin considerar cohesión

$$e_{ah_1} = \gamma'_v \cdot K_a = 0,49 \cdot 72,00 = 35,28 \text{ kN/m}^2$$

$$e_{ah_1} = 35,28 \text{ kN/m}^2$$

- empuje considerando cohesión

$$e_{ah} = \gamma'_v \cdot K_a - 2 \cdot c \cdot \sqrt{K_a} = 35,28 \text{ kN/m}^2 - 2 \cdot 8 \text{ kN/m}^2 \cdot \sqrt{0,49} = 35,28 \text{ kN/m}^2 - 16 \cdot 0,7 = 35,28 - 11,20 = 24,08 \text{ kN/m}^2$$

- profundidad crítica

$$h_0 = \frac{2 \cdot c}{\gamma} \cdot \tan \left(45^\circ + \frac{\phi'}{2} \right) = \frac{2 \cdot 8 \text{ kN/m}^2}{18 \text{ kN/m}^3} \cdot \tan (45^\circ + 10^\circ) = \frac{16 \text{ m}}{1,8} \cdot 1,428 = 1,27 \text{ m}$$

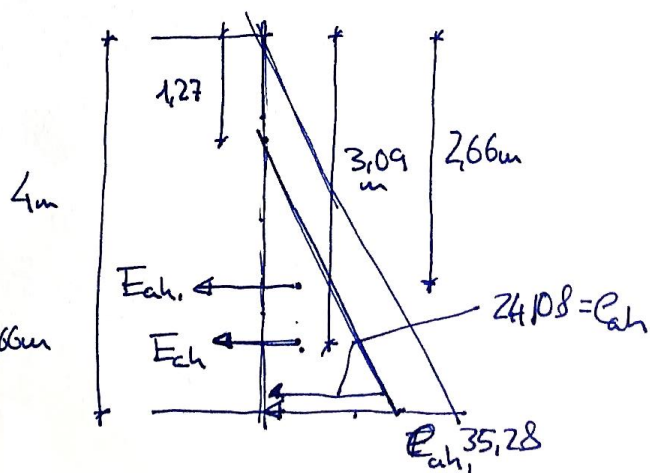
$$h_0 = 1,27 \text{ m}$$

- empujes (resultantes)

$$E_{ah_1} = e_{ah_1} \cdot \frac{4}{2} = 70,56 \text{ kN}$$

$$\text{punto aplicación} = h \cdot \frac{2}{3} = 4 \cdot \frac{2}{3} = 2,66 \text{ m}$$

$$E_{ah} = 24,08 \text{ kN/m}^2 \cdot (4 - h_0) = 24,08 \cdot (4 - 1,27) = 65,73 \text{ kN}$$

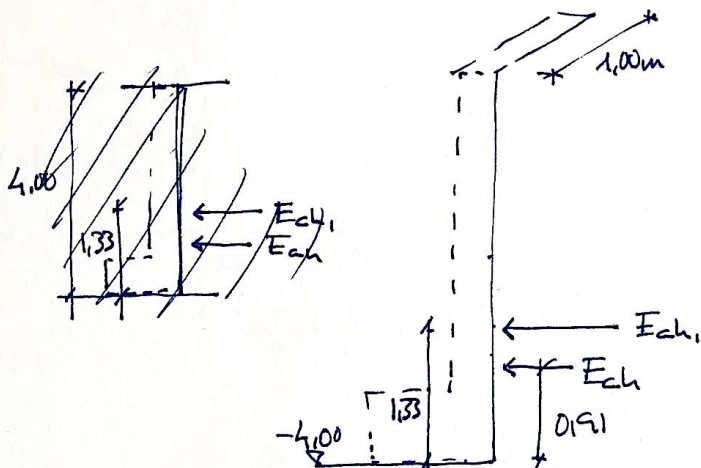


②

cont. E1

$$E_{ch} = 24,08 \text{ kN/m}^2 \cdot \frac{h-h_0}{2} = 24,08 \cdot \frac{4-1,27}{2} =$$

$$E_{ch} = 32,87 \text{ kN}$$



$$M_{d1} = 93,84 \text{ kN}\cdot\text{m}$$

$$M_{d1} = E_{ch1} \cdot 1,33\text{m} = 70,56 \cdot 1,33$$

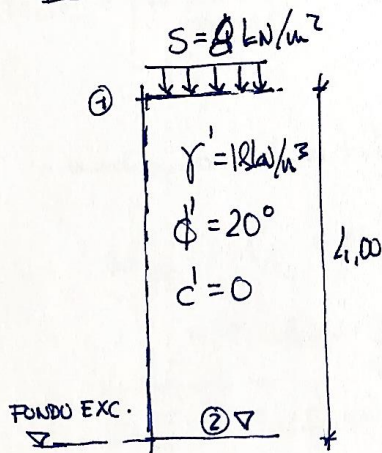
$$= 93,84 \text{ kN}\cdot\text{m}$$



$$M_d = E_{ch} \cdot 0,91\text{m} \approx$$

$$M_d = 29,91 \text{ kN/m}$$

EXERCICIO 2



- calculamos tensiones verticales efectivas

$$\sigma'_{v1} = \sigma_{v1} = S = 8 \text{ kN/m}^2$$

$$\sigma'_{v2} = \sigma_{v2} = S + \gamma' \cdot h = 8 \text{ kN/m}^2 + 18 \text{ kN/m}^3 \cdot 4 \text{ m}$$

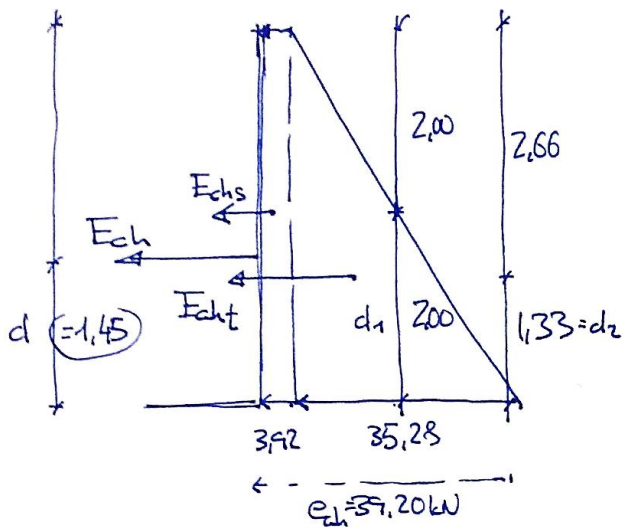
$$\sigma'_{v2} = 80 \text{ kN/m}^2$$

$$K_{ah} = 0,49 \text{ (ej-1)}$$

$$E_{ch1} = \sigma'_{v1} \cdot K_{ah} = 8 \text{ kN/m}^2 \cdot 0,49 = 3,92 \text{ kN/m}^2$$

$$E_{ch2} = \sigma'_{v2} \cdot K_{ah} = 80 \text{ kN/m}^2 \cdot 0,49 = 39,20 \text{ kN/m}^2$$

cont. E_z



$$E_{chs} = 3,92 \text{ kN/m}^2 \cdot 4 \text{ m} = 15,68$$

$$E_{chs} = 15,88 \text{ kN}$$

$$E_{chf} = 35,28 \text{ kN/m}^2 \cdot 4 \text{ m} \cdot \frac{1}{2} \quad \text{ejercicio 1}$$

$$E_{chf} = 70,56 \text{ kN}$$

$$E_{ch} = E_{chs} + E_{chf} = 15,88 \text{ kN} + 70,56 \text{ kN}$$

$$E_{ch} = 86,44 \text{ kN}$$

- momento empuje resp. a terreno sin sobrecarga

$$\% \Delta E = \left[\frac{86,44 \text{ kN} - 70,56}{70,56} \right] \times 100 = \frac{15,88}{70,56} \times 100 = 22,51\%$$

- momento desestabilizador

$$M_d = M_{ds} + M_{dt} = E_s \cdot d_1 + E_t \cdot d_2 =$$

$$= 15,88 \text{ kN} \cdot 2 \text{ m} + 70,56 \text{ kN} \cdot 1,33 \text{ m} = 31,76 \text{ kN} \cdot \text{m} + 93,84 \text{ kN} \cdot \text{m}$$

$$M_d = 125,60 \text{ kN} \cdot \text{m}$$

$$\% \Delta M_d = \frac{125,60 - 93,84}{93,84} \times 100 = +33,84\%$$

- punto de aplicación

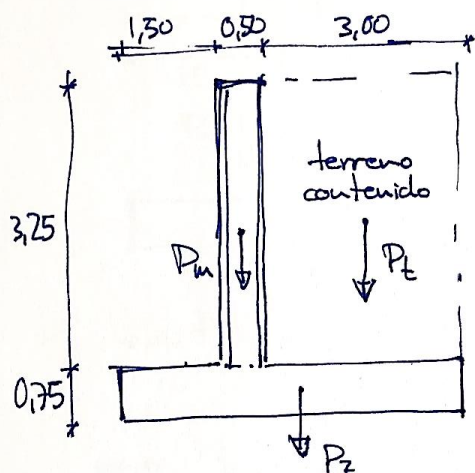
$$M_d = E_s \cdot d_1 + E_t \cdot d_2 = E \cdot d$$

$$d = \frac{M_d}{E} = \frac{125,60 \text{ kN} \cdot \text{m}}{86,44 \text{ kN}} = 1,45 \text{ m}$$

$$d = 1,45 \text{ m}$$

~~comprobación~~

EFERCICIO 3: comprobación deslizamiento



$$P_m = 0,50m \times 3,25 \cdot (1m) \cdot 25 \text{ kN/m}^3 = 40,63 \text{ kN}$$

$$P_z = 3,00 \times 0,75 \cdot (1m) \cdot 25 \text{ kN/m}^3 = 93,75 \text{ kN}$$

$$P_t = 3,00 \times 3,25 \cdot (1m) \cdot 18 \text{ kN/m}^3 = 175,50 \text{ kN}$$

$$\Sigma F_v = P_m + P_z + P_t = 309,88 \text{ kN}$$

caso 1: $E_{ch} = 70,56 \text{ kN}$ (sin sobrecarga)

$$F_d = \frac{\Sigma F_v \cdot \tan \delta'}{E_{ch}} = \frac{309,88 \cdot \tan 13,33^\circ}{70,56} = \frac{309,88 \cdot 0,237}{70,56} = 1,04$$

$$\delta' = \frac{2}{3} \phi' = \frac{2}{3} \cdot 20^\circ = 13,33^\circ \rightarrow \tan 13,33^\circ = 0,237$$

$F_d = 1,04 \leq 1,50 \rightarrow$ no desliza, pero tiene un coeficiente de seguridad muy escaso y un riesgo muy alto.

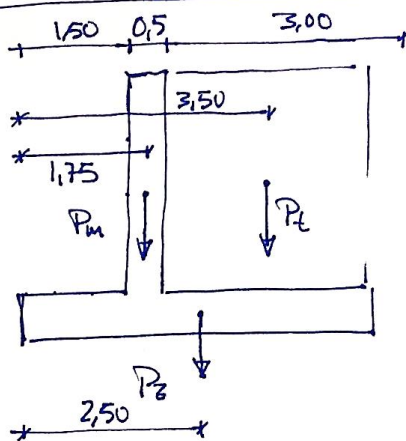
caso 2: $E_{ch} = 86,44 \text{ kN}$

$$F_d = \frac{\Sigma F_v \cdot \tan \delta'}{E_{ch}} = \frac{309,88 \cdot 0,237}{86,44} = 0,85$$

$$\boxed{F_d = 0,85 \leq 1} \rightarrow \text{el muro deslizaría}$$

(5)

Ej. 3: comp. vuelco



$$M_{eskab.} = P_m \cdot 1,75m + P_z \cdot 2,50m + P_t \cdot 3,50m$$

$$M_{est.} = 40,63 \cdot 1,75 + 93,75 \cdot 2,50 + 175,50 \cdot 3,50$$

$$= 71,10 + 234,38 + 614,25$$

$$M_{est} = 919,73 \text{ kN} \cdot m$$

caso 1

$$M_{des.} = E_{ch} \cdot d = 70,56 \cdot 1,33 = 93,84 \text{ kN}$$

$$F_{v1} = \frac{919,73}{93,84} = 9,80 \quad \boxed{F_{v1} > 1,5} \quad (\text{mucho mayor})$$

caso 2 (de ejercicio 2)

$$M_{des.} = 125,60 \text{ kN}$$

$$F_{v2} = \frac{919,73}{125,60} = 7,32 \quad \boxed{F_{v2} > 1,5}$$

$$F_{v1} = \frac{919,73}{93,84} = 9,80 \quad F_{v2} = \frac{919,73}{125,60} = 7,32$$

conclusión el problema, en este caso, es el deslizamiento del muro en su base. Habría que pensar en otras estrategias para maximizar su resistencia al deslizamiento y hacer una zapata de menor dimensión.

