

# 11 – Introduction to Gust / Turbulence Dynamic Response

## Part 2: Continuous Turbulence response

Vibraciones y Aeroelasticidad

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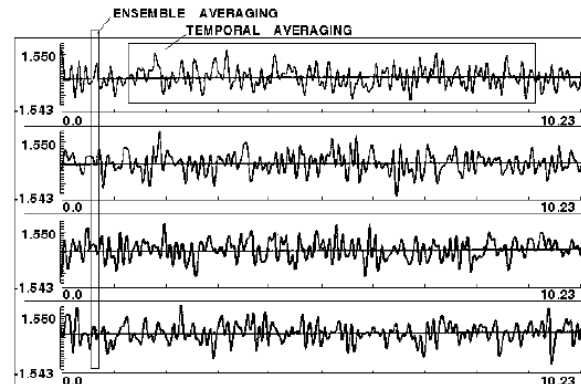
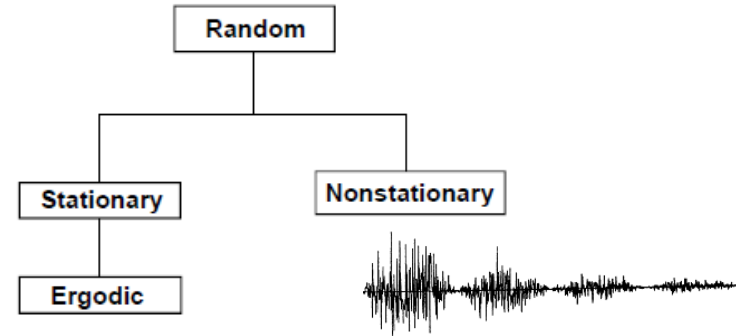
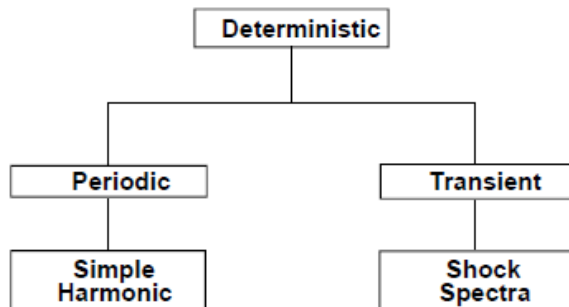
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ESCUELA TÉCNICA SUPERIOR DE INGENIERÍA AERONÁUTICA Y DEL ESPACIO

# DYNAMIC ENVIRONMENTS

## DETERMINISTIC vs RANDOM



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- ❑ Random phenomenon can be described only in a statistical sense. Its instantaneous magnitude at any time is not known; rather, the probability of its magnitude exceeding a certain value is given
  
- ❑ Examples include earthquake ground motion, ocean wave heights and frequencies, wind pressure fluctuations on aircraft and tall buildings, and acoustic excitation due to rocket and jet engine noise
  
- ❑ Characterization of a random signal:
  - ▶ Root Mean Square
  - ▶ Cumulative Mean Square
  - ▶ Power Spectral Density



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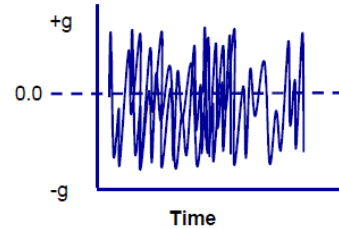
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# RANDOM SIGNALS

## Root Mean Square “RMS” and Cumulative Mean Square “CMS”

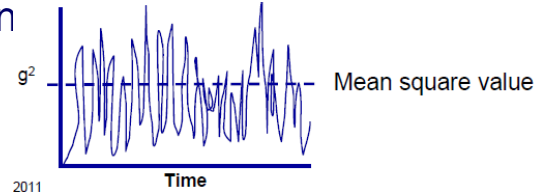


- Assume random signal with zero mean value:



- Square the signal to get a non-zero mean

- Non-zero mean value = mean square

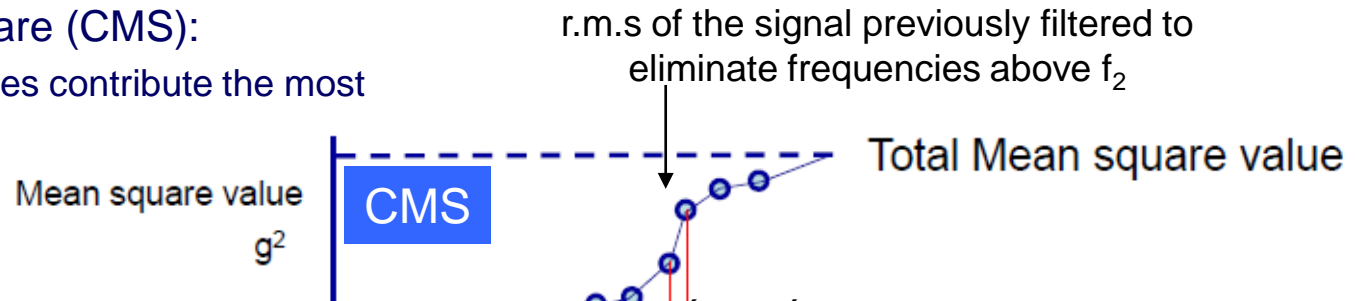


- It can be shown that the “Square Root of the Mean Square” (RMS) value is:

- Equal to the standard deviation  $\sigma$  of a Normal Distribution  $\rightarrow$  value that has 68.3% chance of occurring
- “3  $\sigma$ ” gives a probability of 99.73% chance of occurring

- Cumulative Mean Square (CMS):

- Show which frequencies contribute the most



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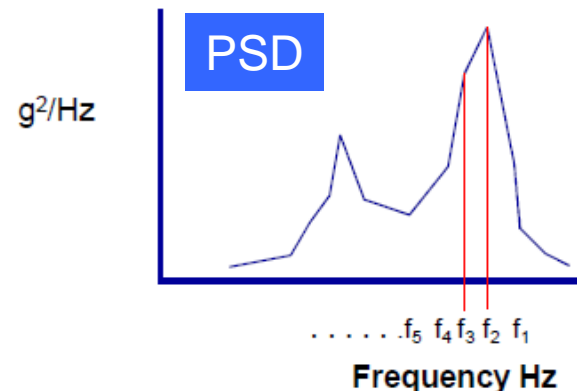
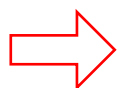
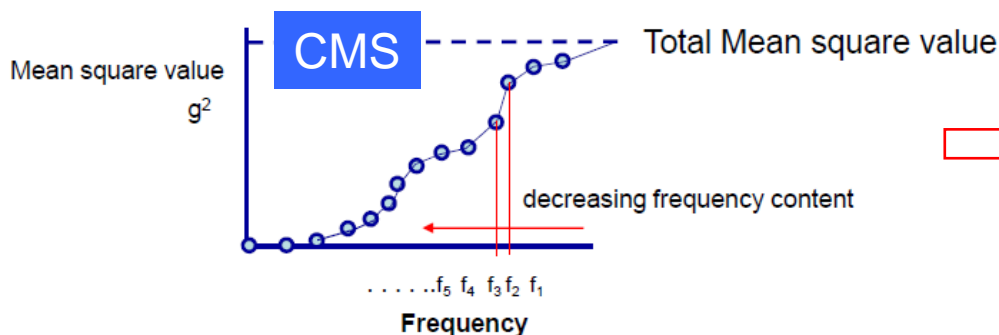
Frequency

# RANDOM SIGNALS

## POWER SPECTRAL DENSITY "PSD"



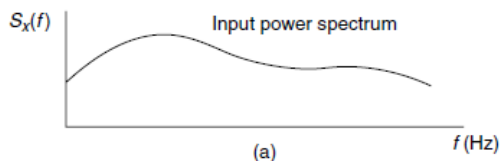
Now take the gradient of the CMS:



- ▶ The PSD shows the frequency content of the signal more directly than the CMS plot
- ▶ **The square root of the area under the PSD curve is the RMS !**

Key point on using PSD in IN-OUT random processes :

- ▶ "OUTPUT" PSD is related to the "INPUT" PSD thru Frequency Response Function H(f)



$$S_y(f) = |H(f)|^2 \cdot S_x(f)$$

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f (Hz)

# EXAMPLE OF ANALYSIS OF RANDOM SIGNALS

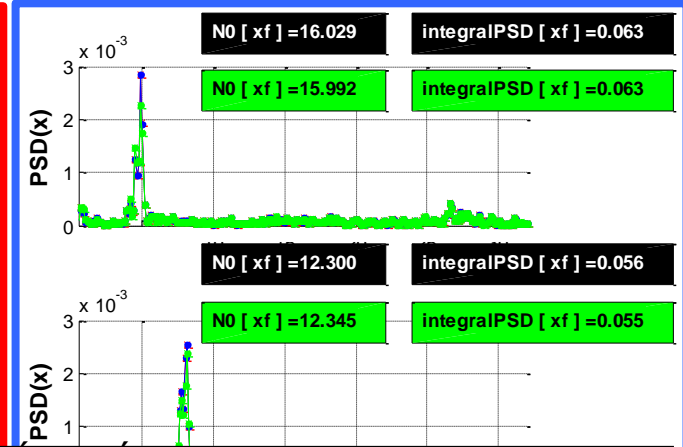
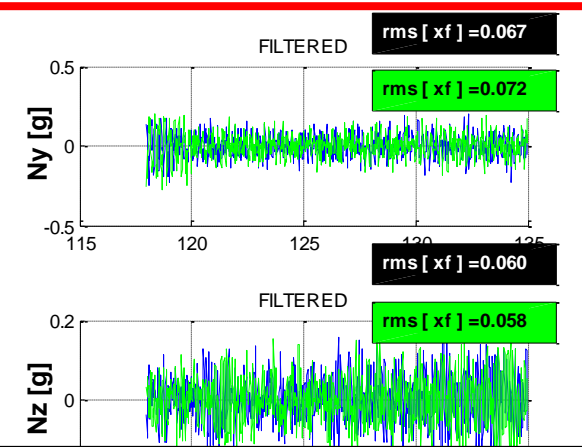
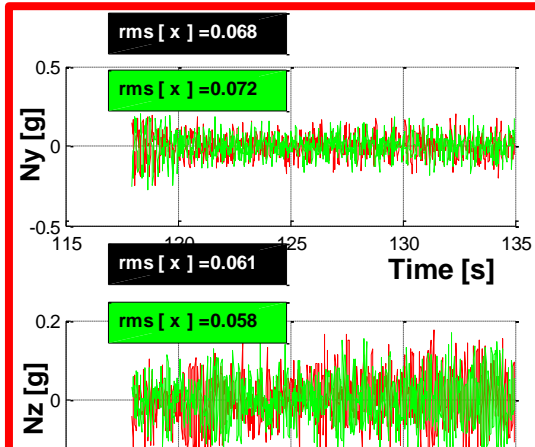
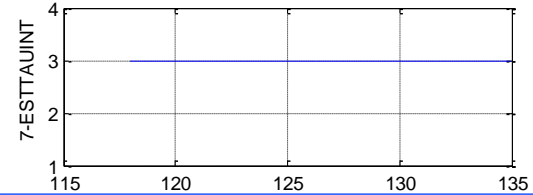
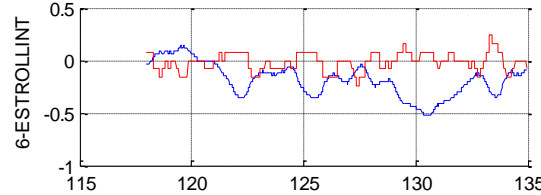
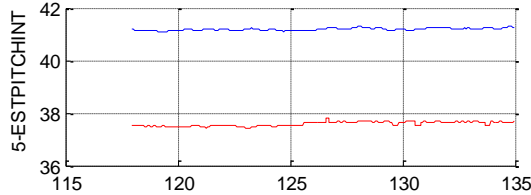
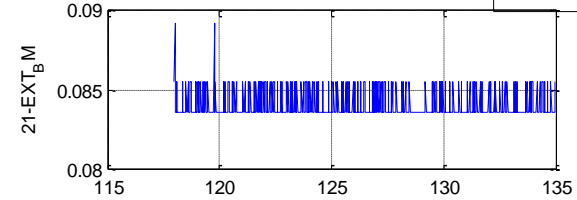
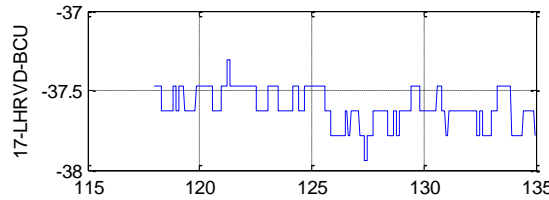
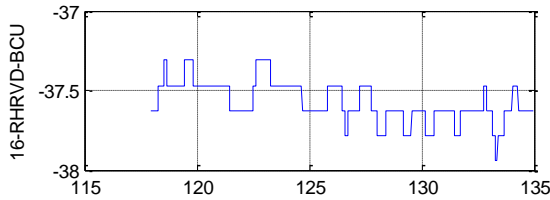


KCAS =324 / MACH =0.82 / ALT[ft]=27807 / EXT[m] =0.08

max PITCH =41.31

max ROLL =0.15

f382r008



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# “GAUSSIAN” OR “NORMAL” DISTRIBUTION

VALUES WITH PROBABILITY 1/1000



$$\Phi_I(\Omega) = \frac{L}{\pi} \frac{1 + \frac{8}{3}(1.339\Omega L)^2}{[1 + (1.339\Omega L)^2]^{11/6}}$$

PSD of a  $\sigma_w = 1$  rms  
Random Gust

$$\bar{A}_i = \left[ \int_0^\infty |h_i(\Omega)|^2 \phi_I(\Omega) d\Omega \right]^{1/2}$$

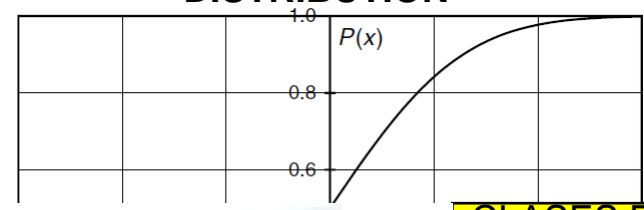
rms of a  
magnitude “i” for a  
turbulence with  
 $\sigma_w = 1$

$$P_{Li} = P_{(1-g)i} \pm P_{Li} = P_{(1-g)i} \pm U_\sigma \bar{A}_i$$

It should be noted that the reference gust velocity is comprised of two components, a root-mean-square (RMS) gust intensity and a peak to RMS ratio.

$$U_\sigma \approx 3 \cdot \sigma_w$$

## PROBABILITY OF A “GAUSSIAN” O “NORMAL” DISTRIBUTION



Probability,  $P(x)$ , of a Gaussian random waveform lying between  $-\infty$  and  $x$ .

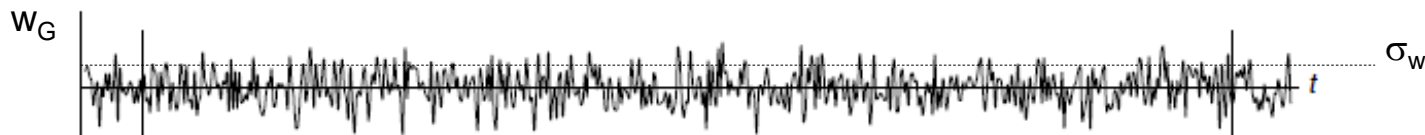
$x/\sigma$	$P(x)$
$-\infty$	0
-3.1	0.0010
-3.0	0.0013
-2.5	0.0062
-2.0	0.0228
-1.5	0.0668
-1.0	0.1587
-0.5	0.3085

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# PSD OF CONTINUOUS TURBULENCE

## Von Karman and Dryden Models



### Von Karman Model

$$\Omega = \frac{\omega}{U_\infty} = \frac{2\pi f}{U_\infty}$$

L = Scale of Turbulence = 2500  
U<sub>∞</sub> = Flight Speed

### Dryden Model

$$\Phi(f) = \sigma_w^2 \frac{2L}{U_\infty} \frac{1 + \frac{8}{3}(1,339L\Omega)^2}{\left[1 + (1,339L\Omega)^2\right]^{\frac{11}{6}}}$$

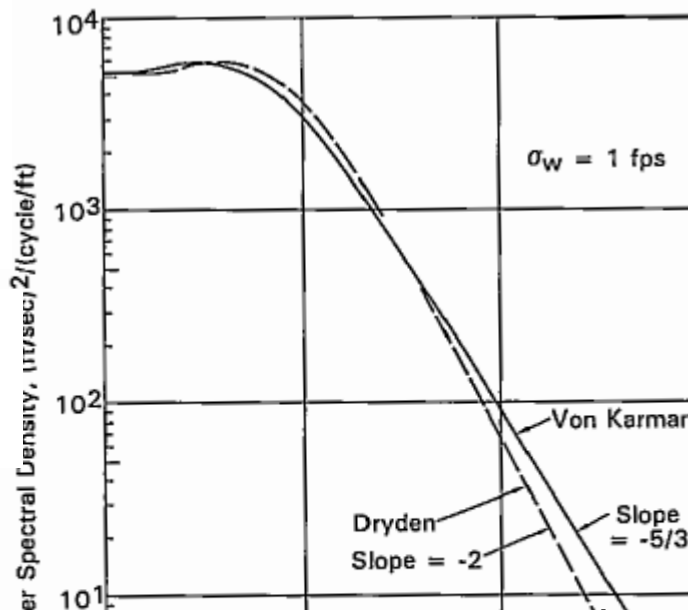
$$\Phi\left(\frac{\Omega}{2\pi}\right) = \sigma_w^2 2L \frac{1 + \frac{8}{3}(1,339L\Omega)^2}{\left[1 + (1,339L\Omega)^2\right]^{\frac{11}{6}}}$$

$$\Phi(\omega) = \sigma_w^2 \frac{L}{\pi U_\infty} \frac{1 + \frac{8}{3}(1,339L\Omega)^2}{\left[1 + (1,339L\Omega)^2\right]^{\frac{11}{6}}}$$

$$\Phi(f) = \sigma_w^2 \frac{2L}{U_\infty} \frac{1 + 3L^2\Omega^2}{(1 + L^2\Omega^2)^2}$$

$$\Phi\left(\frac{\Omega}{2\pi}\right) = \sigma_w^2 2L \frac{1 + 3L^2\Omega^2}{(1 + L^2\Omega^2)^2}$$

$$\Phi(\omega) = \sigma_w^2 \frac{L}{\pi U_\infty} \frac{1 + 3L^2\Omega^2}{(1 + L^2\Omega^2)^2}$$



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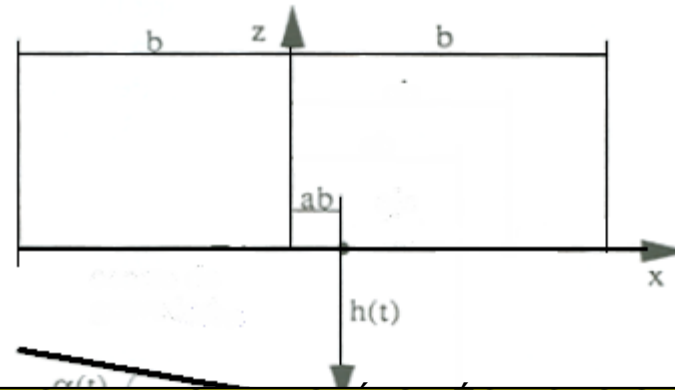
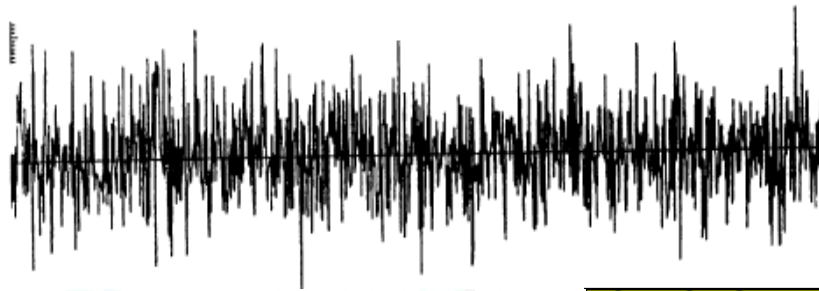
$\frac{\Omega}{2\pi}$  cycles/ft



## NOW... LET'S FIX CONCEPTS WITH OUR TYPICAL SECTION

For the sake of simplicity, let's assume:

- ▶ Incompressible flow (Theodorsen's theory remains applicable)
- ▶ Only heave motion  $h(t)$
- ▶ No stiffness ( $K_h = 0$ ) and zero structural damping ( $g_h = 0$ )



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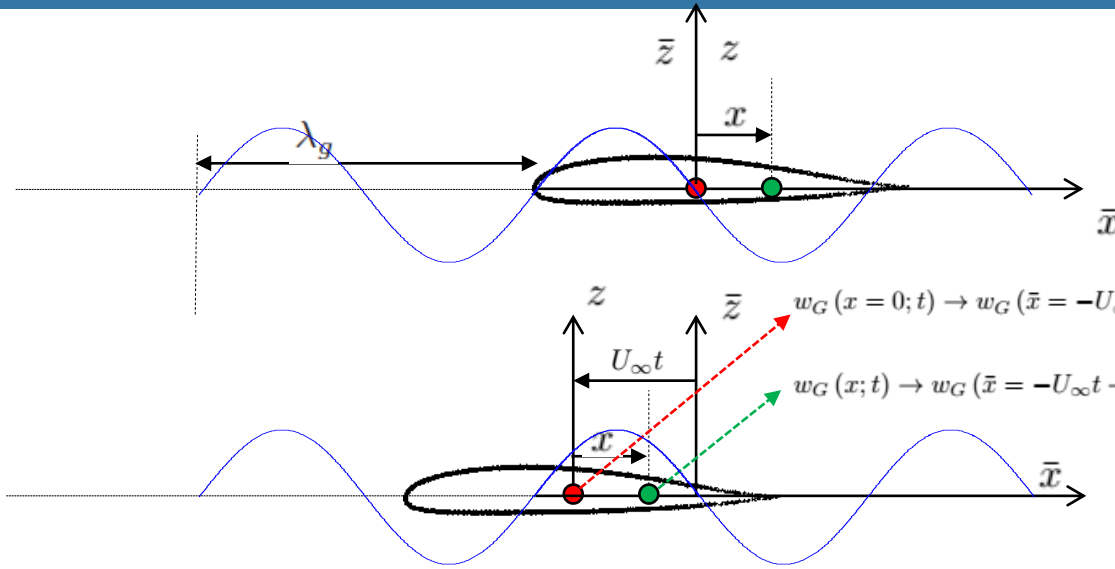
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# CALCULATION OF FREQUENCY RESPONSE FUNCTION (1/3)

## 2D INCOMPRESSIBLE FLOW IN h-MOTION



$$w_G(\bar{x}) = w_0 \sin\left(\frac{2\pi}{\lambda_g} \bar{x}\right)$$

$$w_G(x=0;t) \rightarrow w_G(\bar{x} = -U_\infty t) = w_0 \sin\left(-\frac{2\pi}{\lambda} U_\infty t\right) = w_0 \sin(-\omega t)$$

$$w_G(x;t) \rightarrow w_G(\bar{x} = -U_\infty t + x) = w_0 \sin\left(-\omega t + \omega \frac{x}{U_\infty}\right) \rightarrow w_G = w_0 e^{-i\omega t} e^{+i\omega \frac{x}{U_\infty}}$$

$$w_G(x;t) = w_0 e^{i\omega x/U_\infty} e^{-i\omega t} = \bar{w}_G(x) e^{-i\omega t} \Rightarrow \bar{w}_G(x) = w_0 e^{i\omega x/U_\infty} = w_0 e^{ikx/b}$$

THEODORSEN'S FORMULATION  
(see presentation #19)

$$\frac{\bar{w}(x)}{U_\infty} = -\frac{\bar{w}_G}{U_\infty} = -\frac{w_0}{U_\infty} e^{ikx/b}$$

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# CALCULATION OF FREQUENCY RESPONSE FUNCTION (2/3)

## 2D INCOMPRESSIBLE FLOW IN h-MOTION



$$L_G = 2\pi\rho_\infty U_\infty b \bar{w}_G \{C(k) [J_0(k) - iJ_1(k)] + iJ_1(k)\} e^{iks} = 2\pi\rho_\infty U_\infty b S(k) \bar{w}_G$$
$$L_M = \pi\rho_\infty U_\infty^2 \ddot{h}(s) + 2\pi\rho_\infty U_\infty^2 C(k) \dot{h}(s)$$

$$M \frac{U_\infty^2}{b^2} \ddot{h}(s) = -2\pi\rho_\infty U_\infty b S(k) \bar{w}_G - \pi\rho_\infty U_\infty^2 \ddot{h}(s) - 2\pi\rho_\infty U_\infty^2 C(k) \dot{h}(s)$$

$$\frac{-\omega^2 \bar{h}}{\bar{w}_G} = -\frac{U_\infty}{2b^2} \frac{S(k)}{\lambda + \frac{1}{4} - i\frac{1}{2} \frac{C(k)}{k}} = H(ik)$$

$$\lambda = \frac{M}{4\pi\rho_\infty b^2}$$

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$$\Psi(\omega) = |H(\omega)|^2 \Phi(\omega) = \frac{U_\infty^2}{b^2} \frac{4k^2 |S(k)|^2}{|-(4\lambda + 1)k + 2iC(k)|^2} \sigma_w^2 \frac{L}{\pi U_\infty} \frac{1 + 3 \left(\frac{\omega L}{U_\infty}\right)}{\left[1 + \left(\frac{\omega L}{U_\infty}\right)^2\right]^2}$$

$$kS(k) \approx \frac{1}{1 + 2\pi k} = \frac{\frac{\omega L}{U_\infty} \frac{b}{L}}{1 + 2\pi \frac{\omega L}{U_\infty} \frac{b}{L}}$$

$$|-(4\lambda + 1)k + 2iC(k)|^2 \approx 4 + k^2 (2\lambda + 1)^2 = 4 + \left(\frac{\omega L}{U_\infty}\right)^2 \left(\frac{b}{L}\right)^2 (2\lambda + 1)^2$$

$b / L \rightarrow 0$  Scale of turbulence  $\gg$  characteristic length of the vehicle  $\rightarrow d^2h / dt^2 \approx 0$

$b / L \rightarrow \infty$  Scale of turbulence  $\ll$  characteristic length of the vehicle  $\rightarrow d^2h / dt^2 \approx 0$

$(b / L)_{crit}$  Scale of turbulence associated to maximum vertical acceleration

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### PROBLEMA 1

Determinar el factor de carga de un ala rígida pero libre de desplazarse verticalmente cuando encuentra una ráfaga de intensidad  $w_G(s) = w_0 \cos(\Omega s)$ , siendo  $s = U_\infty t/b$  el tiempo adimensional,  $b$  la semicuerda del ala y las funciones de Wagner y Küssner aproximándose por:

$$\Phi(s) = 1 - 0,165e^{-0,0455s} - 0,335e^{-0,300s}$$

$$\Psi(s) = 1 - 0,500e^{-0,130s} - 0,500e^{-s}$$

Expresar el resultado en función de parámetros adimensionales.

### PROBLEMA 2

Dentro de la validez de la teoría aerodinámica bidimensional, incompresible y no estacionaria, se desea estudiar la respuesta de un puente frente a ráfagas. Para ello se considera una sección característica de anchura  $2b$  y masa por unidad de envergadura  $M$  en presencia de un viento horizontal  $U_\infty$ . Repentinamente, y durante un tiempo  $t_1$ , aparece una velocidad vertical uniforme  $w_0 \ll U_\infty$ . Teniendo en cuenta que tanto el espesor como el desplazamiento vertical de la sección característica son pequeños frente a su anchura, calcular la evolución temporal de la velocidad vertical de la sección, considerando que no gira y que la rigidez a flexión de la sección analizada es  $M\omega_h^2$ .

Dibujar el resultado anterior cuando la masa vale  $M = 4383 \text{ Kg.m}^{-1}$ , la anchura del puente es 4 [m], la rigidez a flexión es nula y la duración de la ráfaga es infinita.



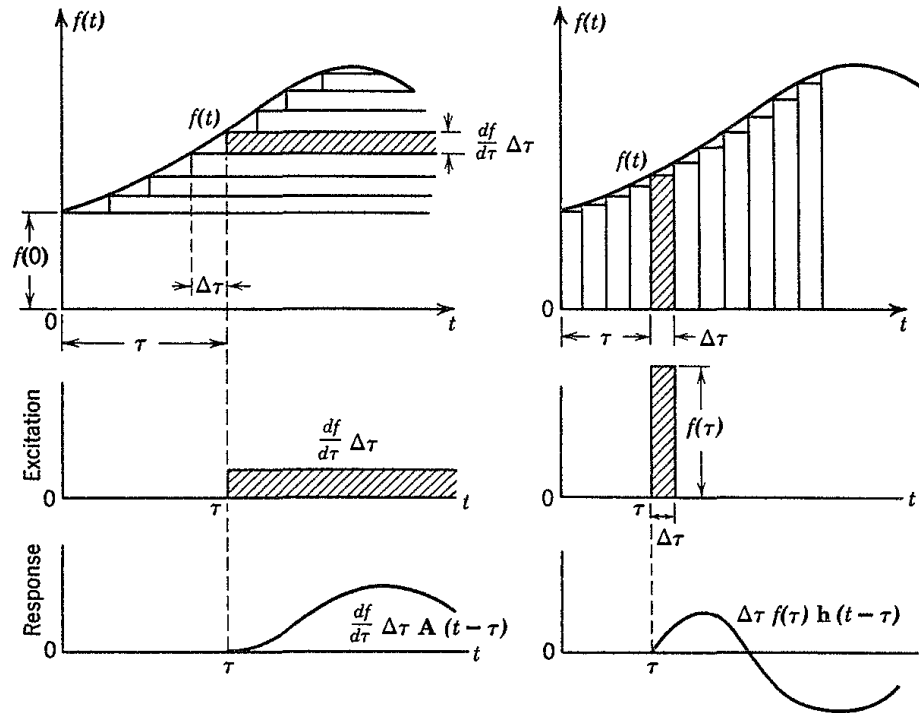
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$x(t)$  response of the physical system to the input  $f(t)$



$A(t)$

“Indicial Admittance” = response to unit-step function

$h(t)$

response to unit-step function

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$dt$

$$\mathcal{L}\{f(t)\} = \int_0^{\infty} f(t)e^{-st} dt$$

$$\mathcal{L}^{-1}\{F(s)G(s)\} = (f * g)(t)$$

$$(f * g)(t) = \int_{-\infty}^{\infty} f(t-x)g(x)dx$$



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