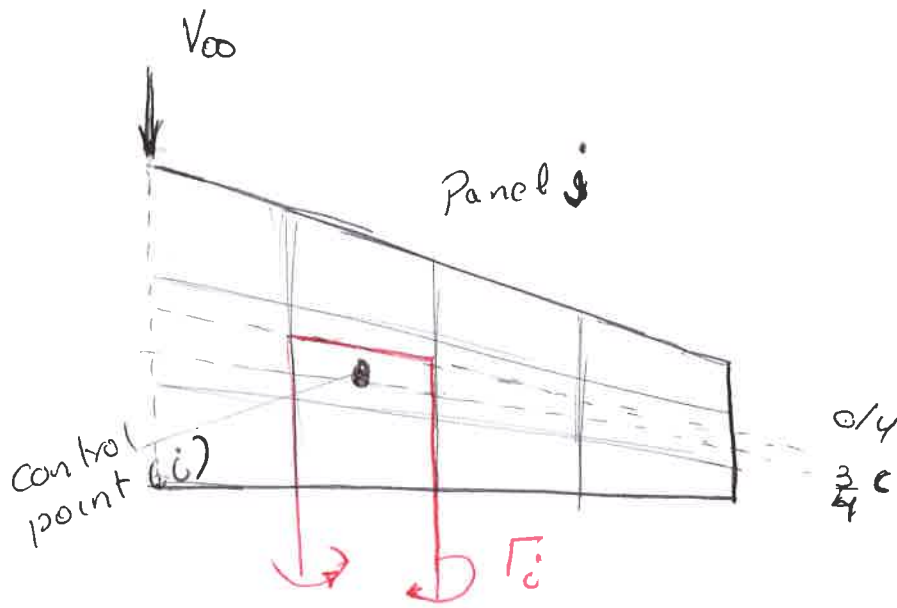


# Vortex Lattice Method

Consider an incompressible, inviscid flow, and the wing is modelled as a set of panels.



Bound vortex is located at panel  $\frac{1}{4}$  chord position with two trailing vortex lines shed from each end.

The required strength of bound vortex on each panel will need to be calculated by applying a surface flow boundary conditions.

The equation to be used is the condition of zero flow normal to the surface.



(2)

The normal velocity is made up of a free stream component and an induced flow component. We know that this induced component is a function of strengths of the all vortex panels on the wing.

$$V_n = 0 = V_{\infty} \sin(\theta) + w_i$$

$$w_j = \sum_{i=1}^N A_{ij} \Gamma_i$$

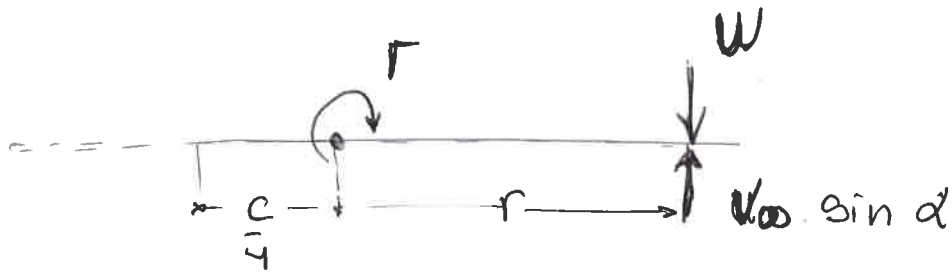
$$-V_{\infty} \sin(\theta) = \sum_{i=1}^N A_{ij} \Gamma_i$$

$A_{ij}$  = Influence coefficient of induced flow on panel (i) due to the vortex on panel (j)

This influence coefficient can be calculated as a relatively simple application of Biot-Savart Law along the three component vortex lines.

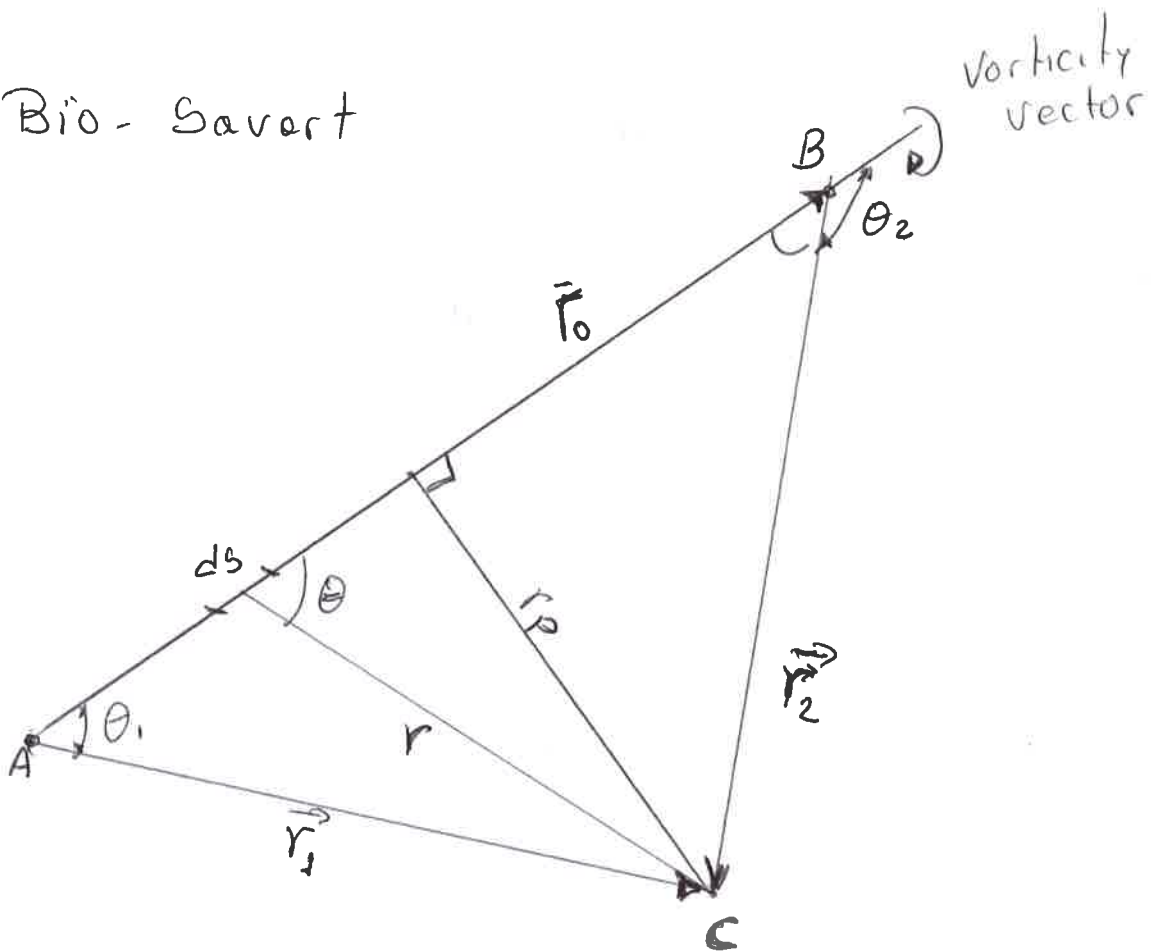
$\alpha$ : small then  $\sin \alpha \approx \alpha$

$$[w_j = -V_{\infty} \alpha]$$



Planar airfoil section indicating location of control point where flow is parallel to the surface.

Biot-Savart



$$d\vec{v} = \frac{1}{4\pi r^3} \Gamma_n (d\vec{L} \times \vec{r})$$

3

$$dV = \frac{\Gamma_n \sin \theta dL}{4\pi r^2}$$

Applying to obtain the flow field induced by a horseshoe vortex which consists in three straight segments. Let AB be a segment, with the vorticity vector directed from A to B. Let C be a point in space whose normal distance from line AB is  $r_p$ .

$$V = \frac{\Gamma_n}{4\pi r_p} \int_{\theta_1}^{\theta_2} \sin \theta \cdot d\theta = \frac{\Gamma_n}{4\pi r_p} (\cos \theta_1 - \cos \theta_2)$$

For  $\theta_1 = 0$  and  $\theta = \pi$ , the vortex filament extends to infinity in both directions

$$d = \frac{r_p}{\tan \theta} \quad dr = \frac{r_p}{\sin \theta}$$

$$\text{Then } r_p = \frac{|\vec{r}_1 \times \vec{r}_2|}{r_0} \quad \cos \theta_1 = \frac{\vec{r}_0 \cdot \vec{r}_1}{r_0 \cdot r_1}$$

$$\cos \theta_2 = \frac{\vec{r}_0 \cdot \vec{r}_2}{r_0 \cdot r_2}$$

The direction of the induced velocity is given by the unit vector of the ~~cross product~~ of  $\vec{r}_1$  and  $\vec{r}_2$ .

$$\frac{\vec{r}_1 \times \vec{r}_2}{|\vec{r}_1 \times \vec{r}_2|}$$

Unit vector  
direction of induced  
velocity. vector.

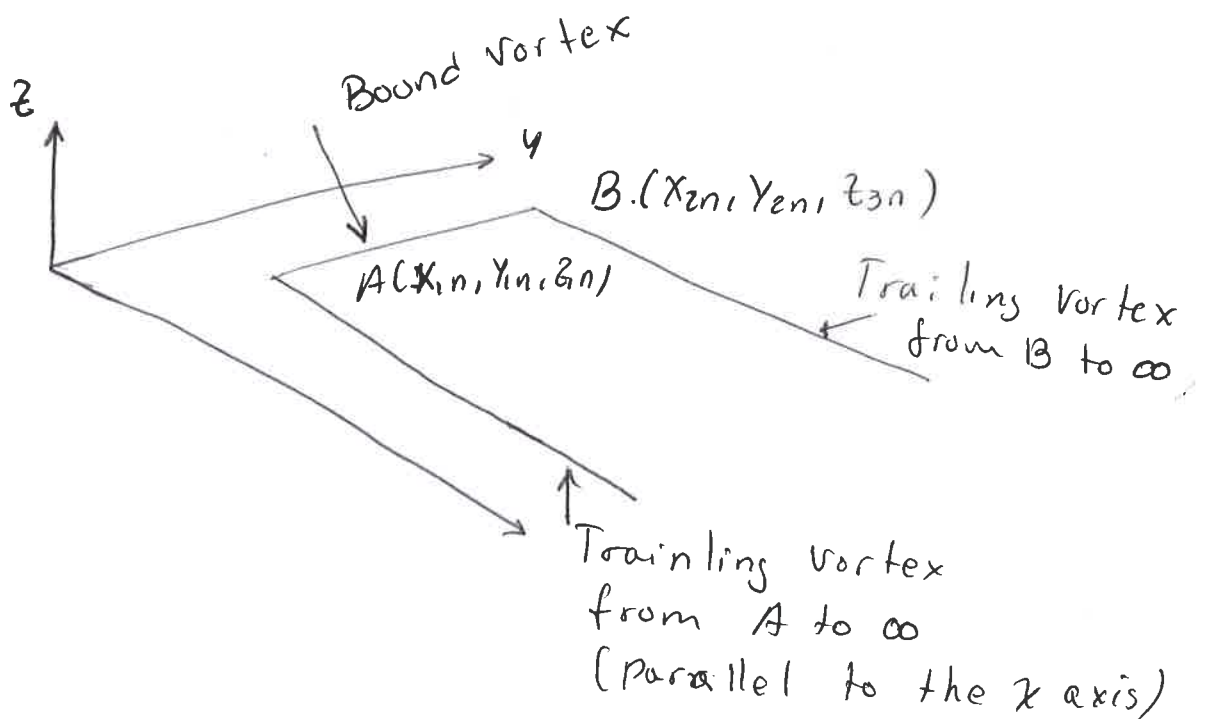
$$\vec{V} = \frac{\Gamma_n}{4\pi} \frac{(\vec{r}_1 \times \vec{r}_2)}{|\vec{r}_1 \times \vec{r}_2|} \frac{1}{r_0} \left[ \frac{\vec{r}_0 \cdot \vec{r}_1}{r_0 r_1} - \frac{\vec{r}_0 \cdot \vec{r}_2}{r_0 r_2} \right]$$

$$\vec{V} = \frac{\Gamma_n}{4\pi} \frac{(\vec{r}_1 \times \vec{r}_2)}{|\vec{r}_1 \times \vec{r}_2|^2} \left[ r_0 \left( \frac{\vec{r}_1}{r_1} - \frac{\vec{r}_2}{r_2} \right) \right]$$

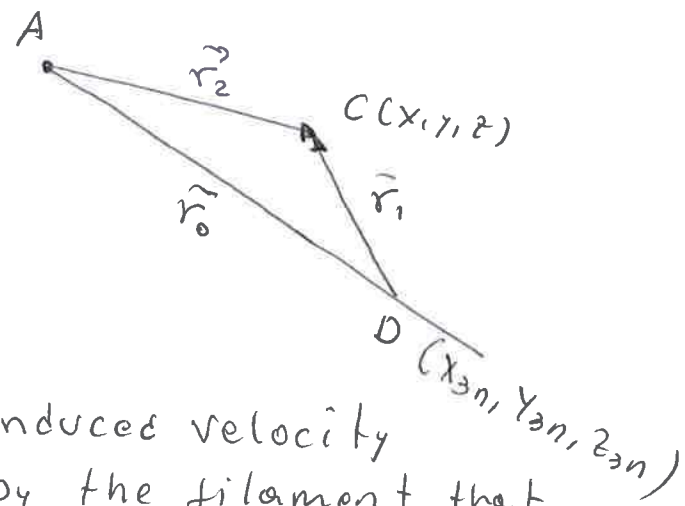
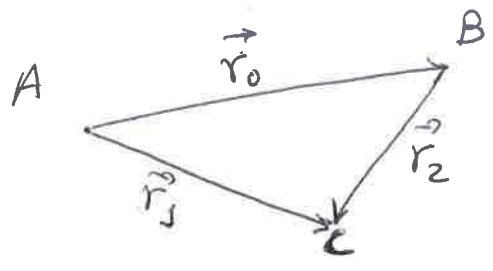
$$\vec{r}_0 = \vec{AB} = (x_{2n} - x_{1n})\hat{i} + (y_{2n} - y_{1n})\hat{j} + (z_{2n} - z_{1n})\hat{k}$$

$$\vec{r}_1 = (x - x_{1n})\hat{i} + (y - y_{1n})\hat{j} + (z - z_{1n})\hat{k}$$

$$\vec{r}_2 = (x - x_{2n})\hat{i} + (y - y_{2n})\hat{j} + (z - z_{2n})\hat{k}$$



Using the above equation the velocity induced at point C (x, y, z) by the vortex filament AB.



Induced velocity by the filament that extends from A to ∞.

$$\vec{V}_{AB} = \frac{\Gamma_n}{4\pi} \{Fac1_{AB}\} \{Fac2_{AB}\}$$

$$\begin{aligned} \{Fac1_{AB}\} &= \frac{\vec{r}_1 \times \vec{r}_2}{|\vec{r}_1 \times \vec{r}_2|^2} \\ &= \{ [(y - y_{1n})(z - z_{2n}) - (y - y_{2n})(z - z_{1n})] \hat{i} \\ &\quad - [(x - x_{1n})(z - z_{2n}) - (x - x_{2n})(z - z_{1n})] \hat{j} \\ &\quad + [(x - x_{1n})(y - y_{2n}) - (x - x_{2n})(y - y_{1n})] \hat{k} \} / \\ &\quad \{ [(y - y_{1n})(z - z_{2n}) - (y - y_{2n})(z - z_{1n})]^2 \\ &\quad + [(x - x_{1n})(z - z_{2n}) - (x - x_{2n})(z - z_{1n})]^2 \\ &\quad + [(x - x_{1n})(y - y_{2n}) - (x - x_{2n})(y - y_{1n})]^2 \} \end{aligned}$$

and

$$\{\text{Fac2}_{AB}\} = \left( \vec{r}_0 \cdot \frac{\vec{r}_1}{r_1} - \vec{r}_0 \cdot \frac{\vec{r}_2}{r_2} \right)$$

$$= \left\{ \frac{[(x_{2n} - x_{1n})(x - x_{1n}) + (y_{2n} - y_{1n})(y - y_{1n}) + (z_{2n} - z_{1n})(z - z_{1n})]}{\sqrt{(x - x_{1n})^2 + (y - y_{1n})^2 + (z - z_{1n})^2}} \right. \\ \left. - \frac{[(x_{2n} - x_{1n})(x - x_{2n}) + (y_{2n} - y_{1n})(y - y_{2n}) + (z_{2n} - z_{1n})(z - z_{2n})]}{\sqrt{(x - x_{2n})^2 + (y - y_{2n})^2 + (z - z_{2n})^2}} \right\}$$

For  $\vec{DA}$

$$\vec{r}_0 = \vec{DA} = (x_{1n} - x_{3n})\hat{i}$$

$$\vec{r}_1 = (x - x_{3n})\hat{i} + (y - y_{1n})\hat{j} + (z - z_{1n})\hat{k}$$

$$\vec{r}_2 = (x - x_{1n})\hat{i} + (y - y_{1n})\hat{j} + (z - z_{1n})\hat{k}$$

$$V_{AD} = \frac{\Gamma_n}{4\pi} \left[ (\text{Fac1}_{AD}) (\text{Fac2}_{AD}) \right]$$

where

$$\{\text{Fac1}_{AD}\} = \frac{(z - z_{1n})\hat{j} + (y_{1n} - y)\hat{k}}{[(z - z_{1n})^2 + (y_{1n} - y)^2](x_{3n} - x_{1n})}$$

and

$$\{\text{Fac2}_{AD}\} = (x_{3n} - x_{1n}) \left\{ \frac{x_{3n} - x}{\sqrt{(x - x_{3n})^2 + (y - y_{1n})^2 + (z - z_{1n})^2}} \right. \\ \left. + \frac{x - x_{1n}}{\sqrt{(x - x_{1n})^2 + (y - y_{1n})^2 + (z - z_{1n})^2}} \right\}$$

Letting  $x_3$  go to  $\infty$ , the first term of  $(\text{Fac2}_{AD})$  goes to 1.0, the velocity induced by the vortex filament which extends from  $A$  to  $\infty$  in a positive direction parallel to the  $x$ -axis is given.



$$\vec{V}_{A\infty} = \frac{\Gamma_n}{4\pi} \left\{ \frac{(z - z_{1n})\hat{j} + (y_{1n} - y)\hat{k}}{[(z - z_{1n})^2 + (y_{1n} - y)^2]} \right\} \left[ 1.0 + \frac{x - x_{1n}}{\sqrt{(x - x_{1n})^2 + (y - y_{1n})^2 + (z - z_{1n})^2}} \right]$$

Induced Velocity from B to  $\infty$

$$\vec{V}_{B\infty} = -\frac{\Gamma_n}{4\pi} \left\{ \frac{(z - z_{2n})\hat{j} + (y_{2n} - y)\hat{k}}{[(z - z_{2n})^2 + (y_{2n} - y)^2]} \right\} \left[ 1.0 + \frac{x - x_{2n}}{\sqrt{(x - x_{2n})^2 + (y - y_{2n})^2 + (z - z_{2n})^2}} \right]$$

Then the velocity induced at the  $i$ th. control point. by the vortex representing the  $j$ th. panel will be designated as

$W_{ij}$ . Examining equation,

$$\vec{W}_{ij} = \vec{A}_{ij} \cdot \Gamma_n$$

where  $\vec{A}_{ij}$  depend on the geometry of  $j$ th. horseshoe vortex and its distance from the control point  $i$ th. Since the governing equations are linear, the velocities induced by the  $2N$  vortices are added together to obtain an expression for the total induced velocity at the  $i$ th control point.

$$\vec{W}_i = \sum_{n=1}^{2N} \vec{A}_{ij} \cdot \Gamma_n$$