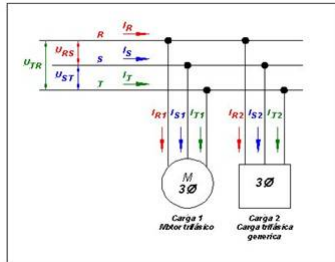




SISTEMAS TRIFÁSICOS

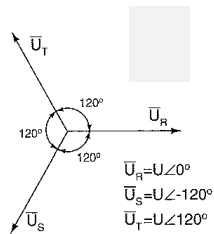


INTRODUCCIÓN

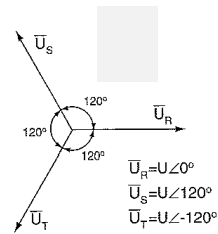
Sistema trifásico :3 magnitudes senoidales

Equilibrado:

1. Mismo módulo
2. Desfasadas 120°



a) Secuencia directa



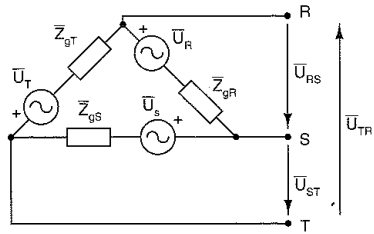
b) Secuencia inversa

Equilibrado

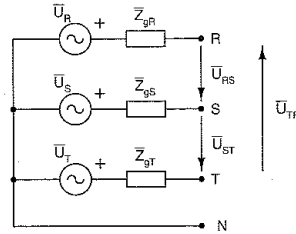
1. $|\vec{U}_R| = |\vec{U}_S| = |\vec{U}_T|$
2. $\vec{U}_R + \vec{U}_S + \vec{U}_T = 0$



GENERADORES TRIFÁSICOS



a) Conexión en triángulo



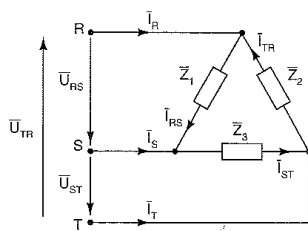
b) Conexión en estrella

Equilibrado

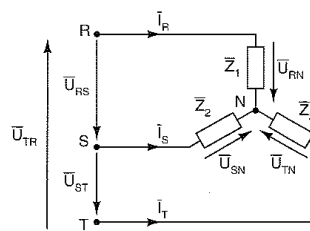
1. $\vec{Z}_{gR} = \vec{Z}_{gS} = \vec{Z}_{gT}$
2. $|\vec{U}_R| = |\vec{U}_S| = |\vec{U}_T|$
3. $\vec{U}_R + \vec{U}_S + \vec{U}_T = 0$



CARGAS TRIFÁSICAS



a) Carga en triángulo



b) Carga en estrella

Equilibrado

$$\vec{Z}_1 = \vec{Z}_2 = \vec{Z}_3$$



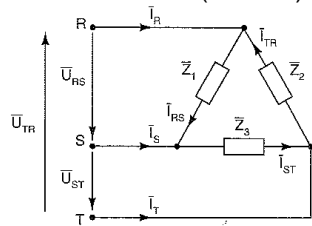
MAGNITUDES DE LINEA Y DE FASE

Tensión simple o de fase (U_F): Diferencia de potencial entre cada una de las ramas monofásicas (módulo)

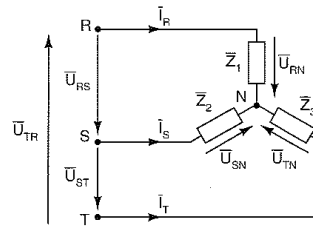
Tensión compuesta o de línea (U_L): Diferencia de potencial entre dos conductores de línea (módulo)

Intensidad de fase (I_F): Intensidad que circula por cada una de las ramas monofásicas I (módulo)

Tensión compuesta o de línea (U_L): Intensidad que circula por cada conductor de línea (módulo)



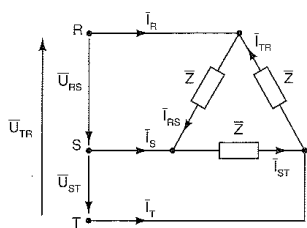
a) Carga en triángulo



b) Carga en estrella



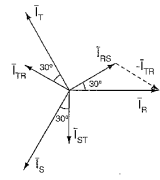
CONEXIÓN TRIÁNGULO EQUILIBRADO



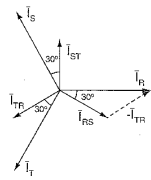
$$U_L = |\vec{U}_{RS}| = |\vec{U}_{ST}| = |\vec{U}_{TR}| = U_F$$

$$I_F = |\vec{I}_{RS}| = |\vec{I}_{ST}| = |\vec{I}_{TR}|; \quad I_L = |\vec{I}_R| = |\vec{I}_S| = |\vec{I}_T|$$

$$\begin{aligned} \vec{I}_R &= \vec{I}_{RS} - \vec{I}_{TR} \\ \vec{I}_S &= \vec{I}_{ST} - \vec{I}_{RS} \\ \vec{I}_T &= \vec{I}_{TR} - \vec{I}_{ST} \end{aligned}$$



a) Secuencia directa



b) Secuencia inversa

$$\vec{I}_R = 2\vec{I}_{RS} \cos(30^\circ)_{(-30^\circ)}$$

$$\vec{I}_R = 2\vec{I}_{RS} \cos(30^\circ)_{(30^\circ)}$$

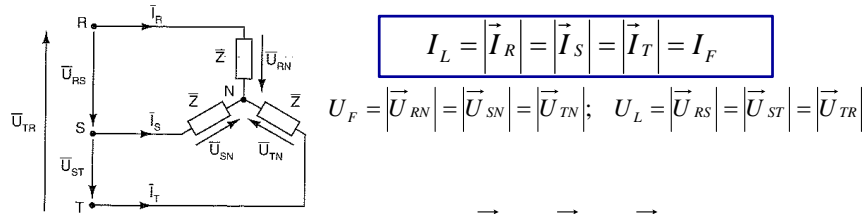
$$\vec{I}_R = \vec{I}_{RS} \sqrt{3}_{(-30^\circ)}$$

$$\vec{I}_R = \vec{I}_{RS} \sqrt{3}_{(30^\circ)}$$

$$I_L = \sqrt{3} I_F$$

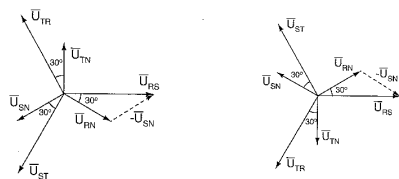


CONEXIÓN ESTRELLA EQUILIBRADA



$$I_L = \vec{I}_R = \vec{I}_S = \vec{I}_T = I_F$$

$$U_F = |\vec{U}_{RN}| = |\vec{U}_{SN}| = |\vec{U}_{TN}|; \quad U_L = |\vec{U}_{RS}| = |\vec{U}_{ST}| = |\vec{U}_{TR}|$$



a) Secuencia directa

b) Secuencia inversa

$$\begin{aligned} \vec{U}_{RS} &= \vec{U}_{RN} - \vec{U}_{SN} \\ \vec{U}_{ST} &= \vec{U}_{SN} - \vec{U}_{TN} \\ \vec{U}_{TR} &= \vec{U}_{TN} - \vec{U}_{RN} \end{aligned}$$

$$U_L = \sqrt{3} U_F$$

$$\vec{U}_{RS} = 2\vec{U}_{RN} \cos(30^\circ) \angle_{30^\circ}$$

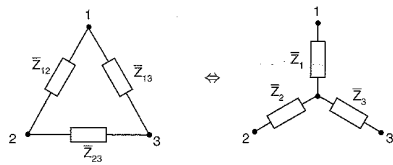
$$\vec{U}_{RS} = 2\vec{U}_{RN} \cos(30^\circ) \angle_{-30^\circ}$$

$$\vec{U}_{RS} = \vec{U}_{RN} \sqrt{3} \angle_{30^\circ}$$

$$\vec{U}_{RS} = \vec{U}_{RN} \sqrt{3} \angle_{-30^\circ}$$



CONVERSIÓN ESTRELLA-TRIÁNGULO



$$\vec{Z}_1 = \frac{\vec{Z}_{12} \vec{Z}_{13}}{\vec{Z}_{12} + \vec{Z}_{13} + \vec{Z}_{23}}$$

$$\vec{Z}_{12} = \vec{Z}_1 + \vec{Z}_2 + \frac{\vec{Z}_1 \vec{Z}_2}{\vec{Z}_3}$$

Equilibrado:

$$\vec{Z}_1 = \vec{Z}_2 = \vec{Z}_3$$

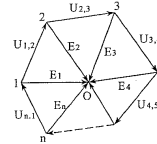
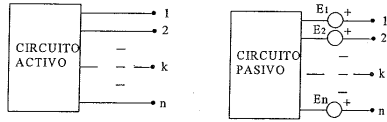
$$\vec{Z}_{12} = \vec{Z}_{23} = \vec{Z}_{13}$$

$$\vec{Z}_Y = \frac{\vec{Z}_\Delta}{3}$$

$$\vec{Z}_\Delta = 3\vec{Z}_Y$$

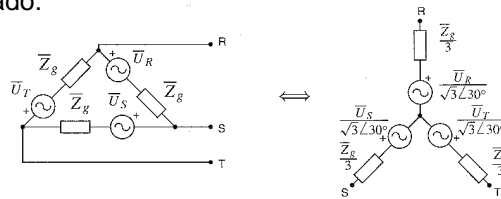


CONVERSIÓN ESTRELLA-TRIÁNGULO

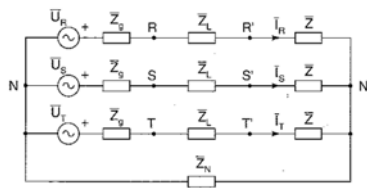


- Thévenin polifásico:
1. Circuitos pasivos iguales
 2. Tensiones compuestas iguales

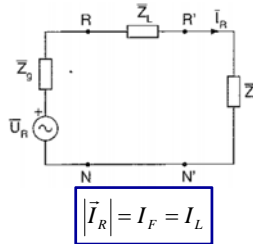
Equilibrado:



RESOLUCIÓN DE SISTEMAS TRIFÁSICOS EQUILIBRADOS CONEXIÓN Y-Y



$$\vec{U}_{NN'} = \frac{\vec{U}_R}{\vec{Z}_g + \vec{Z}_L + \vec{Z}} + \frac{\vec{U}_S}{\vec{Z}_g + \vec{Z}_L + \vec{Z}} + \frac{\vec{U}_T}{\vec{Z}_g + \vec{Z}_L + \vec{Z}} = 0$$



$$\vec{U}_R = \vec{I}_R (\vec{Z}_g + \vec{Z}_L + \vec{Z})$$

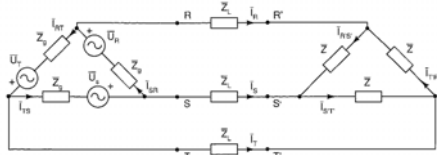
$$\vec{U}_S = \vec{I}_S (\vec{Z}_g + \vec{Z}_L + \vec{Z})$$

$$\vec{U}_T = \vec{I}_T (\vec{Z}_g + \vec{Z}_L + \vec{Z})$$

$$|\vec{I}_R| = I_F = I_L$$



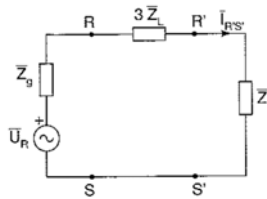
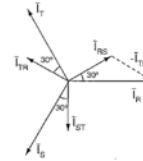
RESOLUCIÓN DE SISTEMAS TRIFÁSICOS EQUILIBRADOS CONEXIÓN Δ-Δ



$$\vec{I}_{SR}\vec{Z}_g - \vec{U}_R + \vec{I}_R\vec{Z}_L + \vec{I}_{R'S'}\vec{Z} - \vec{I}_S\vec{Z}_L = 0$$

$$\left. \begin{aligned} \vec{I}_R &= \vec{I}_{SR} \cdot \sqrt{3} \angle -30^\circ \\ \vec{I}_R &= \vec{I}_{R'S'} \cdot \sqrt{3} \angle -30^\circ \end{aligned} \right\} \vec{I}_{SR} = \vec{I}_{R'S'}$$

$$\left. \begin{aligned} \vec{I}_R &= \vec{I}_{SR} \cdot \sqrt{3} \angle -30^\circ \\ \vec{I}_S &= \vec{I}_{SR} \cdot \sqrt{3} \angle -150^\circ \end{aligned} \right\} \vec{I}_R - \vec{I}_S = 3\vec{I}_{SR}$$



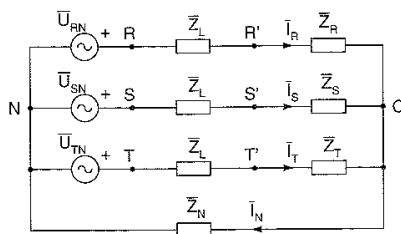
$$\vec{U}_R = \vec{I}_{R'S'} (\vec{Z}_g + 3\vec{Z}_L + \vec{Z})$$

$$\vec{I}_{R'S'} = \vec{I}_F = \vec{I}_L \cdot \frac{1}{\sqrt{3}} \angle -30^\circ$$



RESOLUCIÓN DE SISTEMAS TRIFÁSICOS

- Si es posible se reduce el circuito a una configuración **estrella-estrella**, mediante transformaciones estrella triángulo y asociaciones serie paralelo
- Después se aplica el **Th de Millman** para obtener la caída de tensión entre los nudos de las dos estrellas
- A partir de aquí se pueden obtener las **corrientes de línea** y las **tensiones de fase**



$$\vec{U}_{ON} = \frac{\frac{\vec{U}_{RN}}{\vec{Z}_R + \vec{Z}_L} + \frac{\vec{U}_{SN}}{\vec{Z}_S + \vec{Z}_L} + \frac{\vec{U}_{TN}}{\vec{Z}_T + \vec{Z}_L}}{\frac{1}{\vec{Z}_R + \vec{Z}_L} + \frac{1}{\vec{Z}_S + \vec{Z}_L} + \frac{1}{\vec{Z}_T + \vec{Z}_L} + \frac{1}{\vec{Z}_N}}$$

$$\vec{U}_{RO} = \vec{U}_{RN} - \vec{U}_{ON}$$

$$\vec{I}_R = \frac{\vec{U}_{RO}}{\vec{Z}_L + \vec{Z}_R}$$



POTENCIA EN SISTEMAS TRIFÁSICOS

Potencia instantánea

$$p(t) = p_1(t) + p_2(t) + p_3(t)$$

$$p_i(t) = u_i(t) \cdot i_i(t)$$

Potencia activa (media)

$$P = P_{F1} + P_{F2} + P_{F3}$$

$$P_{Fi} = U_{Fi} \cdot I_{Fi} \cdot \cos \varphi_{Fi}$$

Potencia reactiva

$$Q = Q_{F1} + Q_{F2} + Q_{F3}$$

$$Q_{Fi} = U_{Fi} \cdot I_{Fi} \cdot \text{sen} \varphi_{Fi}$$

Potencia compleja

$$\vec{S} = \vec{S}_{F1} + \vec{S}_{F2} + \vec{S}_{F3} = P + jQ$$

$$\vec{S}_{Fi} = \vec{U}_{Fi} \cdot \vec{I}_{Fi}^* = P_{Fi} + jQ_{Fi}$$

Potencia aparente

$$S = |\vec{S}| = \sqrt{P^2 + Q^2} \neq |\vec{S}_{F1}| + |\vec{S}_{F2}| + |\vec{S}_{F3}| \quad S_{Fi} = |\vec{S}_{Fi}| = U_{Fi} \cdot I_{Fi} = \sqrt{P_{Fi}^2 + Q_{Fi}^2}$$



POTENCIA EN SISTEMAS TRIFÁSICOS EQUILIBRADOS

Potencia instantánea

$$\begin{aligned} p(t) &= p_1(t) + p_2(t) + p_3(t) = \sum_i u_i(t) \cdot i_i(t) = (\dots) \\ &= U_F I_F [3 \cos \varphi + \cos(2\omega t - \varphi) + \cos(2\omega t - 120^\circ - \varphi) + \cos(2\omega t + 120^\circ - \varphi)] = \\ &= 3U_F I_F \cos \varphi \neq f(t) \end{aligned}$$

Potencia activa (media)

$$P = 3U_F \cdot I_F \cdot \cos \varphi$$

Potencia reactiva

$$Q = 3U_F \cdot I_F \cdot \text{sen} \varphi$$

Potencia compleja

$$\vec{S} = 3\vec{S}_F = 3\vec{U}_{Fi} \cdot \vec{I}_{Fi}^* = P + jQ$$

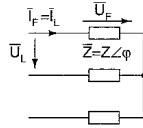
Potencia aparente

$$S = 3S_F = 3U_F \cdot I_F = \sqrt{P^2 + Q^2}$$



POTENCIA EN SISTEMAS TRIFÁSICOS EQUILIBRADOS

Conexión estrella



$$U_L = \sqrt{3} U_F ; I_L = I_F$$

$$P = 3 U_F \cdot I_F \cdot \cos \varphi = \sqrt{3} U_L \cdot I_L \cdot \cos \varphi$$

$$Q = 3 U_F \cdot I_F \cdot \sin \varphi = \sqrt{3} U_L \cdot I_L \cdot \sin \varphi$$

$$\vec{S} = 3 \vec{S}_F = P + jQ =$$

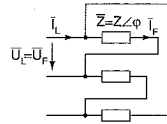
$$= 3 U_F I_F (\cos \varphi + j \sin \varphi) =$$

$$= \sqrt{3} U_L I_L (\cos \varphi + j \sin \varphi)$$

$$S = \sqrt{P^2 + Q^2} = 3 U_F \cdot I_F = \sqrt{3} U_L \cdot I_L$$

$$\vec{S} = 3 \vec{S}_F = 3 \vec{U}_{F_i} \cdot \vec{I}_{F_i}^* = P + jQ \neq \sqrt{3} \vec{U}_{L_i} \cdot \vec{I}_{L_i}^*$$

Conexión triángulo



$$I_L = \sqrt{3} I_F ; U_L = U_F$$

$$P = 3 U_F \cdot I_F \cdot \cos \varphi = \sqrt{3} U_L \cdot I_L \cdot \cos \varphi$$

$$Q = 3 U_F \cdot I_F \cdot \sin \varphi = \sqrt{3} U_L \cdot I_L \cdot \sin \varphi$$

$$\vec{S} = 3 \vec{S}_F = P + jQ =$$

$$= 3 U_F I_F (\cos \varphi + j \sin \varphi) =$$

$$= \sqrt{3} U_L I_L (\cos \varphi + j \sin \varphi)$$

$$S = \sqrt{P^2 + Q^2} = 3 U_F \cdot I_F = \sqrt{3} U_L \cdot I_L$$

$$\vec{S} = 3 \vec{S}_F = 3 \vec{U}_{F_i} \cdot \vec{I}_{F_i}^* = P + jQ \neq \sqrt{3} \vec{U}_{L_i} \cdot \vec{I}_{L_i}^*$$



FACTOR DE POTENCIA

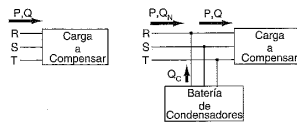
Factor de potencia

$$fdp = \frac{P}{S} = \frac{P}{\sqrt{P^2 + Q^2}}$$

Sistemas equilibrados

$$fdp = \frac{P}{S} = \frac{\sqrt{3} U_L \cdot I_L \cdot \cos \varphi}{\sqrt{3} U_L \cdot I_L} = \cos \varphi$$

Corrección del factor de potencia



$$Q_C = Q - Q_N = P(\operatorname{tg} \varphi - \operatorname{tg} \varphi_N) \quad Q_{CF} = \frac{1}{3} Q_C$$

Condensadores en Y

$$Q_{CF} = \frac{U_F^2}{X_{CY}} = U_F^2 \cdot \omega \cdot C_Y \quad C_Y = \frac{Q_{CF}}{U_F^2 \cdot \omega} = \frac{3Q_{CF}}{U_L^2 \cdot \omega} = \frac{Q_C}{U_L^2 \cdot \omega}$$

Condensadores en Δ

$$Q_{CF} = \frac{U_F^2}{X_{CA}} = U_F^2 \cdot \omega \cdot C_\Delta \quad C_\Delta = \frac{Q_{CF}}{U_F^2 \cdot \omega} = \frac{Q_{CF}}{U_L^2 \cdot \omega} = \frac{Q_C}{3U_L^2 \cdot \omega}$$