

**Table 3
Summary of TE_{mn}^r and TM_{mn}^r mode characteristics of rectangular waveguide**

TE _{mn} ^r ($m = 0, 1, 2, \dots$, $n = n \neq 0$)	TM _{mn} ^r ($m = 1, 2, 3, \dots$, $n = 1, 2, 3, \dots$)
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$$A_{mn} \frac{n\pi}{b\epsilon} \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z} - B_{mn} \frac{m\pi\beta_z}{a\omega\mu\epsilon} \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z}$$

$$-A_{mn} \frac{m\pi}{a\epsilon} \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z} - B_{mn} \frac{n\pi\beta_z}{b\omega\mu\epsilon} \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z}$$

$$0 -jB_{mn} \frac{\beta_c^2}{\omega\mu\epsilon} \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-jkz}$$

$$A_{mn} \frac{m\pi\beta_z}{a\omega\mu\epsilon} \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z} B_{mn} \frac{n\pi}{b\mu} \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z}$$

$$A_{mn} \frac{n\pi\beta_z}{b\omega\mu\epsilon} \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z} - B_{mn} \frac{m\pi}{a\mu} \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z}$$

$$-jA_{mn} \frac{\beta_c^2}{\omega\mu\epsilon} \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta_r z} 0$$

$$\sqrt{\beta_x^2 + \beta_y^2} = \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\beta \sqrt{1 - \left(\frac{f_c}{f}\right)^2}$$

$$\frac{\lambda}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{\lambda}{\sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}}$$

$$\frac{v}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{v}{\sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}}$$

$$\frac{\eta}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{\eta}{\sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}} \quad \eta \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = \eta \sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}$$

$$j \frac{\eta}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = j \frac{\eta}{\sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}} \quad -j\eta \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = -j\eta \sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}$$

TE _{mn} ^r ($m = 0, 1, 2, \dots$, $n = n \neq 0$)	TM _{mn} ^r ($m = 1, 2, 3, \dots$, $n = 1, 2, 3, \dots$)
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$$= \frac{1}{2} \left\{ \left(\epsilon_m + \epsilon_n \frac{b}{a} \right) \left(\frac{f_{c,mn}}{f} \right)^2 - \frac{2R_s}{ab\eta \sqrt{1 - \left(\frac{f_{c,mn}}{f} \right)^2}} \frac{m^2 b^3 + n^2 a^3}{(mb)^2 + (na)^2} \right.$$

$$\left. \frac{m^2 ab + (na)^2}{(mb)^2 + (na)^2} \right\}$$

$$= \begin{cases} 2 & p = 0 \\ 1 & p \neq 0 \end{cases}$$

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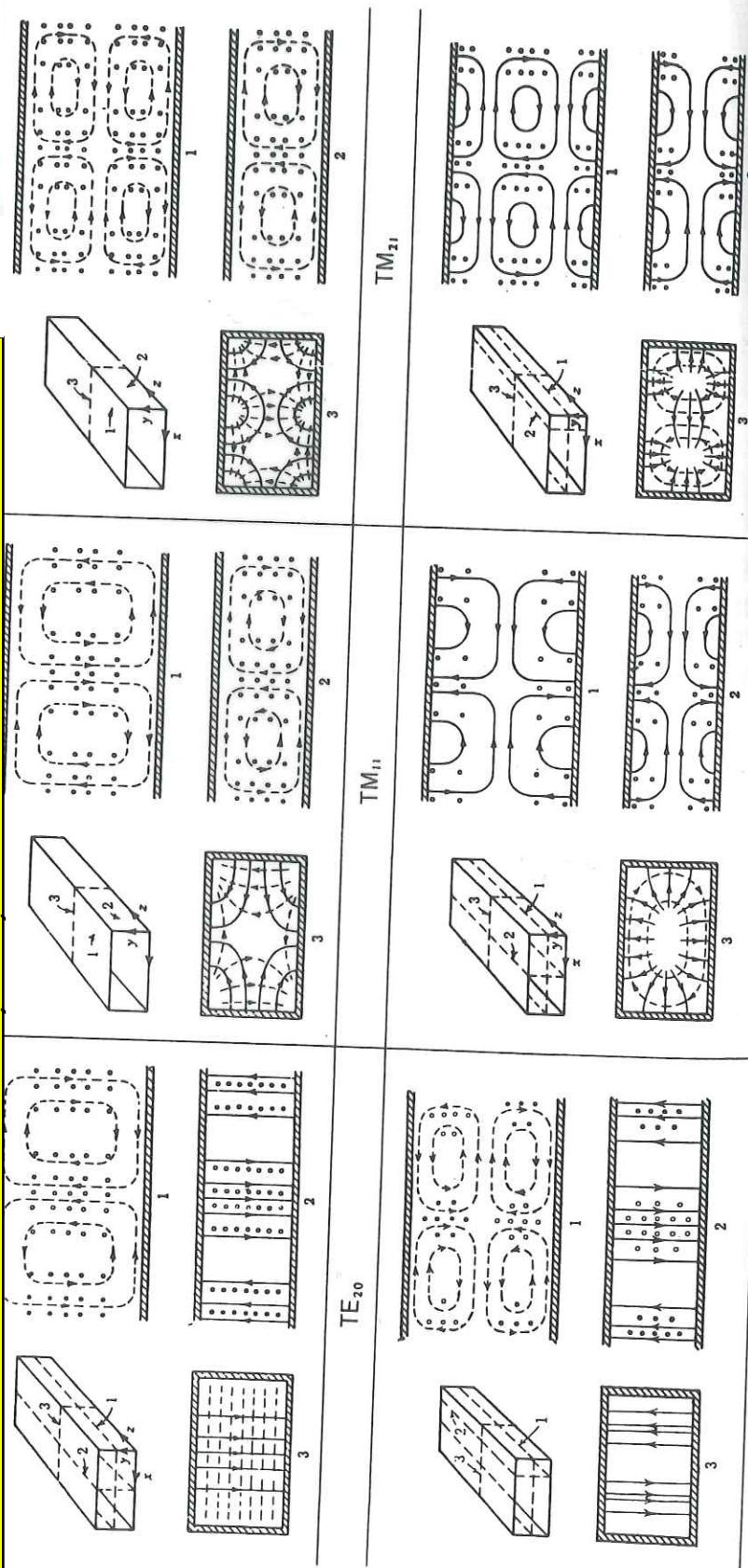
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Solution by the separation

$$H_z = (A'' \sin$$

where

Imposition of boundary conditions and 8.2(14) we find electric

$$\begin{aligned} E_x &= -\frac{j\omega\mu}{k_c^2} \frac{\partial H_z}{\partial y} \\ &= -\frac{j\omega\mu k_y}{k_c^2} \\ E_y &= \frac{j\omega\mu}{k_c^2} \frac{\partial H_z}{\partial x} \\ &= \frac{j\omega\mu k_x}{k_c^2} (A'') \end{aligned}$$

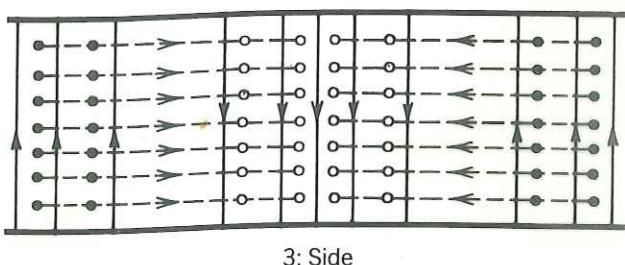
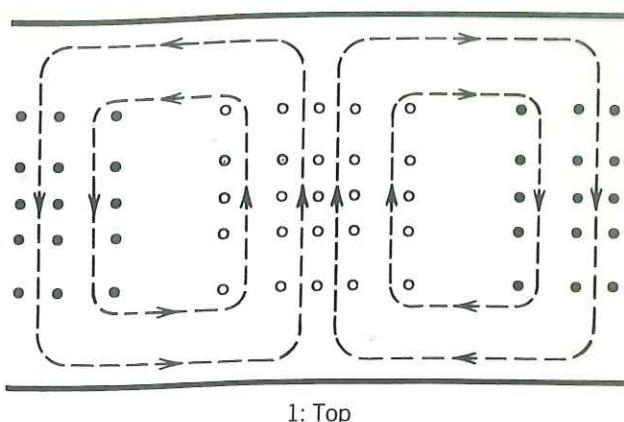
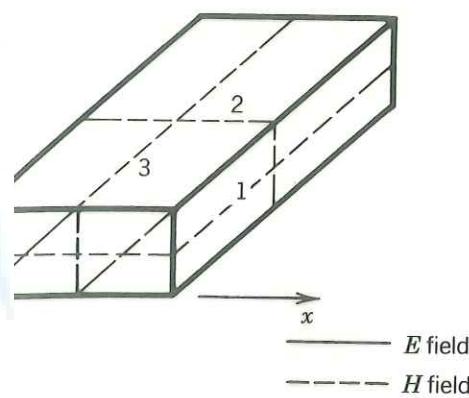
For E_x to be zero at $y = a$, $A'' = 0$. Defining $B''D''$

We also require E_x to be zero at $x = a$ so that $k_x a$ is a

In contrast to the TM wave's vanishing. Although there is no electric field, we can see from the field lines that it is normal to the conductor at $x = a$, so boundary condition requires the explicit form of transverse electric field

The forms of transverse electric field (19) are

* Electric field lines are shown solid and magnetic field lines are dashed.

 TE_{10}

Electric field patterns for TE_{10} mode in a rectangular waveguide (Source: S. Ramo, J. R. Whinnery, and T. Van Duzer, *Fields and Waves in Communication Electronics*, 1984. Reprinted with permission of John Wiley & Sons, Inc.)

From the preceding information it is evident that the electric field intensity inside the guide has only one component, an E_y . The *E*- and *H*-field variations on top, front, and side views of the guide are shown graphically in Figure 8-5, and current density and *H*-field lines on the top and side views are shown in Figure 8-6. It is instructive at this time to examine the electric field intensity a little further and attempt to provide some physical interpretation of the propagation

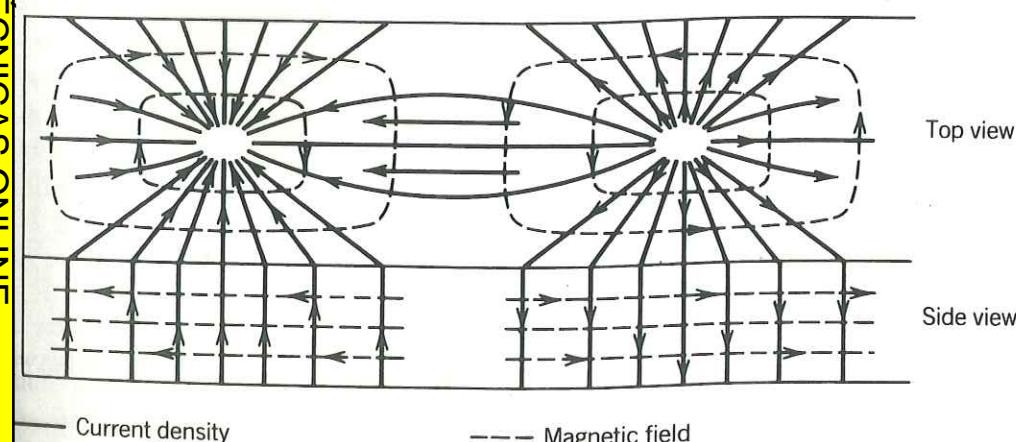


FIGURE 8-6 Magnetic field and electric current density patterns for the TE_{10} mode in a rectangular waveguide. (Source: S. Ramo, J. R. Whinnery, and T. Van Duzer, *Fields and Waves in Communication Electronics*, 1984. Reprinted with permission of John Wiley & Sons, Inc.)

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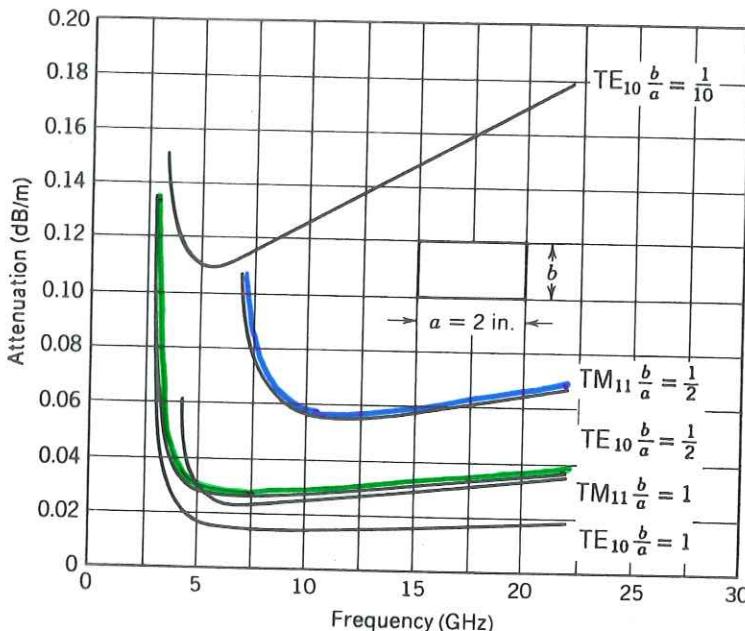


FIG. 8.7c Attenuation due to copper losses in rectangular waveguides of fixed width

The attenuation constant for TE_{mn} ($n \neq 0$) modes is found using power transfer and power loss per unit length as in Eq. 8.5(11).

$$(\alpha_c)_{TE_{mn}} = \frac{2R_s}{b\eta\sqrt{1 - (f_c/f)^2}} \left\{ \left(1 + \frac{b}{a} \right) \left(\frac{f_c}{f} \right)^2 + \left[1 - \left(\frac{f_c}{f} \right)^2 \right] \left[\frac{(b/a)((b/a)m^2 + n^2)}{(b^2m^2/a^2) + n^2} \right] \right\} \quad (26)$$

And for TE_{m0} modes

$$(\alpha_c)_{TE_m0} = \frac{R_s}{b\eta\sqrt{1-(f_c/f)^2}} \left[1 + \frac{2b}{a} \left(\frac{f_c}{f} \right)^2 \right] \quad (27)$$

Figure 8.7c shows attenuation versus frequency for TM_{11} and TE_{10} modes in rectangular copper waveguides with various side ratios b/a found using (14) and (27), respectively. It is seen that small b/a ratios give large attenuations because of the high ratio of surface to cross-sectional area.

8.8 THE TE₁₀ WAVE IN A RECTANGULAR GUIDE

One of the simplest of all the waves which may exist inside hollow-pipe waveguides is the dominant TE_{10} wave in the rectangular guide, which is one of the TE modes

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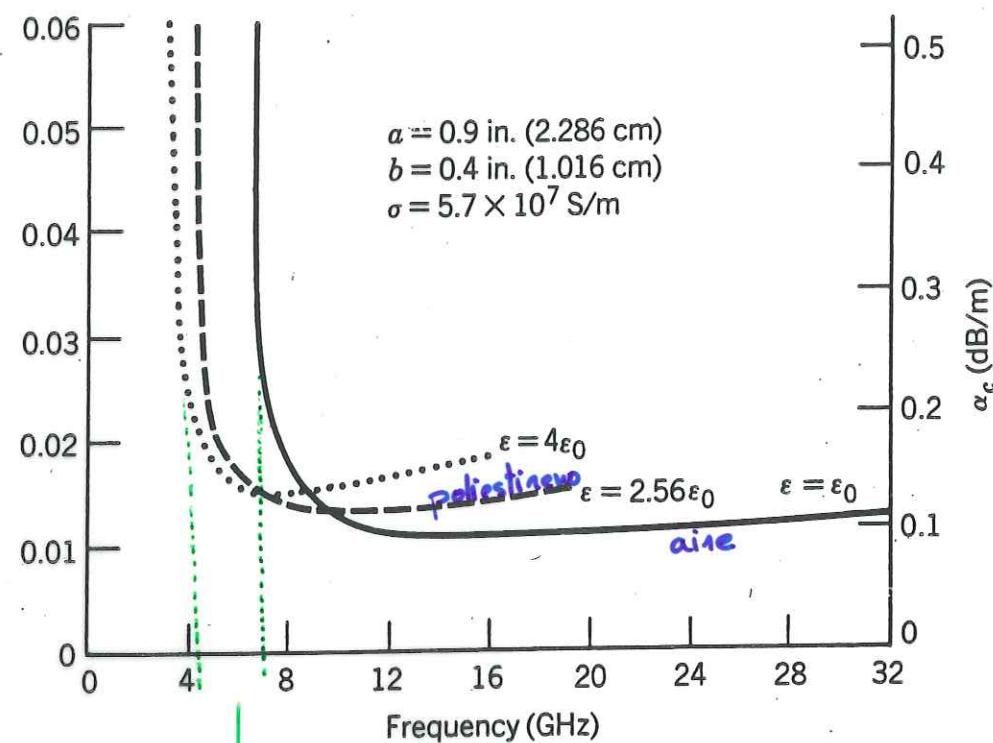


FIGURE 8-10 TE₁₀ mode attenuation constant for the X-band rectangular waveguide.

↓
frecuencias de corte disminuyen cuanto más
"dieléctrico" es el interior de la guía.

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